

Original Research Article

PROPERTIES OF GYPSUM BOARDS MADE OF MIXTURES OF WOOD AND RICE STRAW

ABSTRACT

Aims: It was investigated to produce gypsum-based experimental composite panels with red pine wood/rice straw particles in the mixture up to 40/60 (w/w) in gypsum-water mixture. In this case, the fillers (additives) could be observed more closely.

Methodology: The red pine wood chips and the rice straw (stalks) have been turned into suitable particle dimensions. The experimental boards were cut to determine the IB (Internal bond), MOE–MOR (Modulus of Elasticity and Rupture), and TS (thickness swelling after 24 hours immersion in water). A standard flame combustion test system was conducted according to TS EN-ISO 11925-2. For surface chemical analyses, FTIR was used to evaluate the chemical groups present in the board surface. The thermogravimetric analysis (TGA) was conducted for measuring changes in boards as a function of increasing temperature. The natural weathering tests were conducted that were exposed to outdoor for two months then color and surface hardness tests conducted for determining property changes.

Results: The rice straw had negative impact on thickness swelling (TS) properties of boards in water. The highest TS value of 47.66% was observed in the board that produced from 60/40 (w/w), wood/rice straw mixture (DE4). However, the addition of rice straw to the wood/gypsum mixture has a lowering effect on the internal bond (IB) and bending strength (MOR) properties of experimental boards some level. The maximum IB strength of 0.06 N/mm² and MOR of 2.77 N/mm² found control sample (DE0). However, the highest MOE value of 553 N/mm² was calculated on the DE4 board, which was produced by adding 40% rice straw to the wood/gypsum mixture. In similar trend was also realized for surface hardness properties that the highest hardness (Shore D) value of 44 was observed on the control sample (no rice straw added) while the lowest value of 22 found for DE5 board produced from the mixture of 50/50 (w/w), wood/rice straw. For surface optical properties, the highest total color difference (DE: 8.15), Whiteness reduction (CIE whiteness: -35.48) and Yellowness increasing (E313: 7.03) were found to be control sample (DE0). Some chemical groups are modified to some extent but all relevant chemical groups observed on the FTIR spectra. The addition of rice straw and wood particles to the gypsum structure has a positive effect on the heat transfer properties. The highest insulation value (39.1 °C after 300 second heat application) while the lowest mass loss value of 2.01% was measured in same board (DE6) that produced with the rice straw ratio of 60% in wood-gypsum structure.

Conclusion: It is clear that the addition of rice straw to the wood/gypsum mixture adversely affected the strength properties negatively, but with using some longer fibers may improve the strengths of panels. However rice straw in wood chip/gypsum mixture helps to improve heat resistance (insulation) properties some level. Moreover, the addition of rice straw to wood/gypsum mixture effects on extending hardening time. this is probably gypsum-rice straw interaction that could not effectively wet and penetrate the rice straw surface due to the hydrophobic wax and inorganic silica on the outer surface of rice straw.

Keywords: Rice straw, gypsum board, red pine, strength properties, heat insulation

12 **1. INTRODUCTION**

13

14 Wood has been important raw material sources for housing, energy and decorative
15 purposes. However, in modern times it has become utilized in the fabrication of different
16 products such as pulp and paper products, composite panels, furniture and some chemicals
17 [1, 2]. Due to the excessive use of wood, natural forests have become depleted and of
18 scarcity value. The consumers have also become more aware of the importance of
19 preservation and destruction of the natural forests. Thereby, other alternatives have been
20 studied throughout the world such as agricultural residues or wastes, forest residues, low
21 value woody materials, non-wood materials (annual plants), etc. have been found to be
22 useful as added products instead of wood [3-5]. Moreover, there are numerous literature
23 information for utilization of non-wood sources into processing of products [6-11]. The
24 chemical and physical information on those raw materials and processing into composite
25 manufacturing could be found elsewhere [3, 8, 9].

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27 However, rice stalk or straw is one of the abundant lignocellulosic waste materials in the
28 world. It was stated that 709.2 million tons of wheat straw and 673.3 million tons of rice
29 stalks were exposed worldwide and that large amount of lignocellulosic raw material could
30 be used in the production of composite panels [4]. In more recent study, it was proposed that
31 rice is the third most important grain crop in the world behind wheat and corn. According to
32 FAO statistics, world annual rice production in 2007 was about 650 million tons while every
33 kilogram of grain harvested is accompanied by production of 1–1.5 kg of the straw [12].

34

35 In recent study, it was used the urea-formaldehyde glue as a binder for producing cotton
36 waste-based panels with red pine chips and fibers, separately. It was concluded that in some
37 preparation conditions, it is possible to produce particle- and fiberboards with cotton-based
38 waste materials at acceptable level [13].

39

40 However, gypsum is one of the oldest construction materials throughout human beings. The
41 gypsum based construction and ornamental materials were found ancient civilizations (i.e.
42 Sumerian, Seljuk, Ottoman Aztec, Egyptian, Greek and Roman so on). It was used
43 intensively in Renaissance architecture period in Europe due to its easy shape in interior and
44 exterior spaces by architects and painters [14].

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46 In this study, it was investigated to produce gypsum-based experimental composite panels
47 with red pine wood/rice straw particles in the mixture up to 40/60 (w/w) in gypsum-water
48 mixture. In this case, the fillers (additives) could be observed more closely. Thus, it is
49 possible to produce gypsum-based experimental panels by selecting the most suitable
50 processing conditions.

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52 **2. MATERIAL AND METHODS**

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54 The red pine wood chips were supplied from a local timber company where processing log
55 to timber, Isparta-Turkey. The rice straw (stalks) was supplied from Can-Biga region of
56 Turkey. Both raw materials have been carefully cleaned from dust, bark and other
57 substances then turned into particles through scissors and screened to suitable particle
58 dimensions. The 10-50 mm particles were utilized for adding to gypsum/water mixture. They
59 were then dried at atmospheric conditions until at least a 10-12% moisture content was
60 obtained.

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62 The commercial grade perlite plaster type Gypsum, used as binder agent, supplied by a
63 local company, Isparta Turkey. After manufacturing, the experimental boards, they were
64 conditioned at 20°C and 65% relative humidity. The detailed description of cellulosic raw

65 materials, gypsum with their specifications, and manufacturing process could be found
66 elsewhere [14].

67
68 A total of 14 boards (two for each condition) were made. The experimental procedure for
69 manufacturing experimental particle boards as follows:

- 70 • Press temperature (°C): Ambient temperature
- 71 • Pressing time (day): up to 14
- 72 • Press pressure (N/mm²): 0.1-1.0
- 73 • Wood particles/rice stalk ratio (w/w,%): 100-40/0-60
- 74 • Board dimensions (mm): 400x400x10 cm.
- 75 • Target density (gr/cm³): 0.75 (± 0.1).

76
77 It is important to note that the compatibility of gypsum, red pine particles and rice straw are
78 important but not considered in this study. However, some certain chemicals may also be
79 used to shorten the curing time and improve compatibility of these substances into gypsum.
80 Therefore, only the pure effects of wood/gypsum/rice straw compatibility are considered.

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82 After reaching full strength at ambient temperature, the experimental boards were
83 conditioned at 20 °C and 6 % relative humidity and samples were cut to determine the IB
84 (Internal bond), MOE–MOR (Modulus of Elasticity and Rupture), TS (thickness swelling after
85 24 hours immersion in water), in accordance with TS EN 310 (1999), TS EN 319 (1999) and
86 TS EN 317 (1999), ASTM D 1037, respectively [15-17].

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88 A standard flame combustion test system was conducted according to TS EN-ISO 11925-
89 2. A visual observation of the sample was made either or not the flame spreads in the
90 vertical direction more than 150 mm above (the flame application point) [19-21]. For surface
91 chemical analyses, FTIR spectrophotometer (A Shimadzu (IR Prestige-21) was used to
92 evaluate the chemical groups present in the board surface. For thermogravimetric analysis
93 (TGA), Perkin Elmer SII instrument was utilized for measuring changes in boards as a
94 function of increasing temperature.

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96 The natural weathering tests were conducted on 50x50x10 mm samples from panels were
97 exposed to outdoor for two months then color and surface hardness tests conducted for
98 determining property changes. The total color differences (ΔE) of the samples were
99 measured by X-Rite SP68 Spectrophotometer using CIE L*, a*, b* standards (1976). The
100 surface hardness properties of both control and weathered samples were measured with a
101 Shore D hardness tester, according to test method of ASTM D2240 standard [22]. The
102 board's code numbers (wood chips and rice straw ratios) with gypsum content at various
103 proportions are given in **Table 1**.

104
105 **TABLE 1.** The proportions and code numbers of gypsum boards

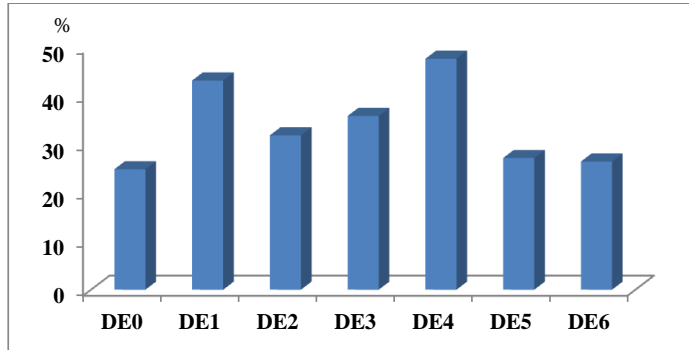
Board code	Wood (gr)	Rice straw (gr)	Wood (%)	Rice straw (%)	Gypsum (gr)
DE0	1000	0	100	0	800
DE1	900	100	90	10	800
DE2	800	200	80	20	800
DE3	700	300	70	30	800
DE4	600	400	60	40	800
DE5	500	500	50	50	800
DE6	400	600	40	60	800

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3. RESULTS AND DISCUSSION

The thickness

117 swelling properties of experimental boards in water are shown in Figure 1. It was realized
 118 that the lowest thickness swelling of 24.85% was observed in the panels produced from the
 119 mixture of wood/gypsum (DE0) (no rice straw added). However, the addition of rice straw to
 120 the mixture had adversely affects the thickness swelling properties. The highest thickness
 121 swelling value of 47.66% found at 60/40 wood/rice straw (w/w) mixture (DE4) condition.
 122 Interestingly, it was realized that the panels include rice straw was equal and/or higher than
 123 the wood chips (DE5 and DE6 boards), the thickness swelling values of 27.18 and 26.45%
 124 were found that only marginally similar to control sample (DE0), respectively.
 125



126 **FIG. 1** Thickness swelling properties of experimental boards in water

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 129 The comparative internal bond (IB) strength properties of experimental boards are shown in
 130 Table 2. The internal bond (IB) strength properties of test boards produced from wood/ rice
 131 straw-gypsum boards were lower than those of the board produced only with wood/gypsum
 132 mixture (DE0). That is, the addition of rice straw to the wood/gypsum mixture has a negative
 133 effect on the IB strengths in all conditions. The maximum IB strength was calculated as 0.06
 134 N/mm² for control sample. In addition, the ANOVA general linear test results showed that the
 135 panels had no statistically difference IB values than each other at 95% confidence level.
 136

137 **TABLE 2** The IB strength properties of gypsum boards

Board code	Density (kg/m ³)	Internal bond (IB) (N/mm ²)	Difference from control (DE0) (%)
DE0	709.99	0.06	0.0
DE1	747.94	0.012	-80.0
DE2	717.94	0.014	-76.7
DE3	719.31	0.015	-75.0
DE4	705.89	0.013	-78.3
DE5	699.70	0.012	-80.0
DE6	697.48	0.011	-81.7

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 139 **The combined effects** of panel density and rice straw additive level on IB properties shown in
 140 **Fig. 2**. As seen, all rice straw addition negatively affects on IB properties some level.
 141 However, increasing panel's density had not much impact on IB of experimental boards.

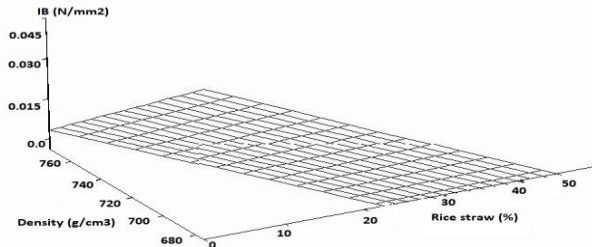


FIG. 2 IB properties of experimental boards.

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The two important mechanical strength properties as a function of the mixture proportion with wood chip/rice straw is shown in Table 3. The bending strength values of the experimental panels (MOR) produced with various proportion additions to rice straw (D1 to D6) was found to be lower than those produced from only wood/gypsum mixture (DE0). This is obviously important in that the introduction of rice straw into the wood/gypsum mixture has the reducing effects on bending strength properties. However, the lowest MOR value was calculated as 0.97 N/mm² in the DE3 panel (70/30; wood chip/rice straw mixture).

The elastic modulus characteristics (MOE) of the boards are also show similar trend. The highest MOE value of 553 N/mm² was calculated on the DE4 board, which was produced by adding 40% rice straw to the wood/gypsum mixture. It was clearly seen that the elastic modulus values of all boards produced by the addition of rice straw into wood/gypsum mixture were improved up to 60/40 wood/rice straw level (w/w), beyond this level the MOE values of experimental panels significantly reduced. In this sense, except a few conditions, the similar situations were also observed for Internal Bond strength (IB) and bending strength (MOR) properties. It could be summarize that the compatibility of rice straw with gypsum is low and should be useful only in controlled conditions or proportions.

The Duncan's multiple range test results also showed that the rice straw and wood chips ratio had some statistically different MOR values that it was in the two for MOR while no statistically difference in MOE values.

TABLE 3 Bending strength and modulus of elasticity of experimental panels

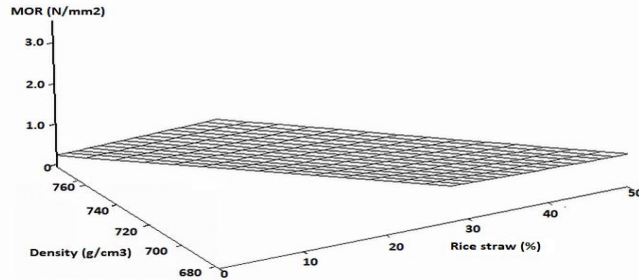
Board Code	MOR (N/mm ²)	Difference from control (%)	MOE (N/mm ²)	Difference from control (%)
DE0	2.77 (B)	0.0	445	0.0
DE1	1.21 (A)	-56.3	113	-74.6
DE2	1.22 (A)	-55.9	192	-56.9
DE3	0.97 (A)	-64.5	443	-0.23
DE4	1.07 (A)	-61.4	553	24.3
DE5	1.16 (A)	-58.1	360	-19.1
DE6	2.30 (B)	-16.9	138	-68.9

168 *Groups with the same letters in each column indicate that there is no statistical difference (P < 0.05) between the
169 samples according to the Duncan's multiple range test.

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The combined effects of both panels density and rice straw ratio impact on bending strength properties of experimental boards are shown in Figure 3. It could be seen that

173 increasing rice straw ratio and panel's density has only marginally effects on panel's MOR
 174 values.
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176 **FIG. 3** Panel density and rice straw ratio effects on the ending strength of experimental
 177 boards
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180 The comparative surface hardness values (Shore D) of the experimental panels are given
 181 in Table 3. The highest Shore D hardness value of 44 was observed on the DE0 type board
 182 while the lowest value of 22 found for DE5 board produced from the mixture of 50:50
 183 wood/rice straw. In general, it is understood that the hardness values of the boards produced
 184 with the increase in rice straw or the decrease in the wood ratio (at fixed the gypsum ratio)
 185 are affected negatively on hardness properties of experimental boards. However, an
 186 interesting situation was encountered that the hardness values of the boards kept under
 187 external atmospheric conditions were found to decrease less than the DE0 sample. The
 188 lowest hardness value reduction in the boards that were kept under external atmospheric
 189 conditions was calculated as 3.2% in DE3 and 4.3% in DE1 type boards, respectively. The
 190 increase in the ratio of rice straw in the mixture adversely affects the hardness values, but it
 191 is important to ensure that the hardness properties of the panels against external
 192 atmospheric conditions remain at a lower trend than control sample (DE0).
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194 However, according to Duncan's multiple range test result, rice straw and wood chips ratio
 195 had some statistically different hardness values that it was in the six statistically different
 196 groups for experimental panels.
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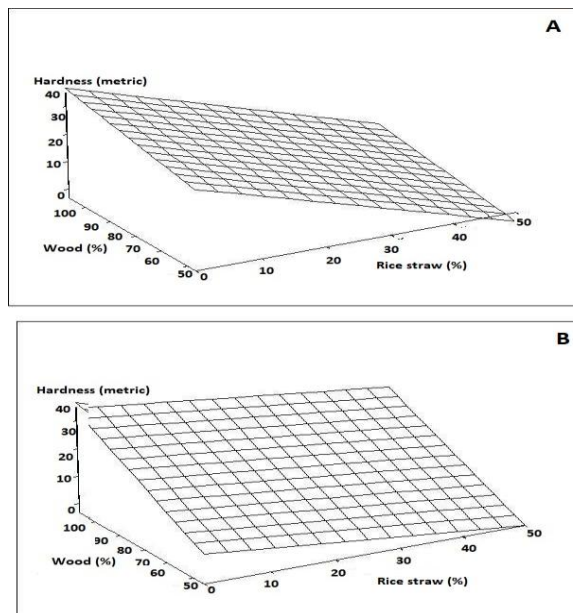
TABLE 4. Surface hardness properties of boards

Board code	Hardness (metric)	Difference from control (DE0) (%)	After weathering hardness (metric)	Changes (%)
DE0	44 (D)	0,0	33	-25
DE1	45 (E)	2.2	43	-4.4
DE2	32 (BC)	-27.2	27	-15.6
DE3	31 (CD)	-29.9	30	-3.2
DE4	23 (A)	-47.8	21	-8.7
DE5	22 (A)	-50.0	20	-9.1
DE6	26 (AB)	-40.9	25	-3.8

198 *Groups with the same letters in each column indicate that there is no statistical difference ($P < 0.05$) between the
 199 samples according to the Duncan's multiple range test.

200 The effects of wood and rice straw ratio on both control and weathered experimental
 201 panels are shown in Figure 4. It was realized that the similar trend was found for both panels

202 that increasing rice stalk ratio or (decreasing wood ratio) negatively effects on experimental
 203 panels.



204 **FIG. 4** Hardness properties of boards (A: Control samples, B: Weathered samples)

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 207 The comparative surface optical (color) properties of boards are shown in Table 5. In
 208 general, it was proposed in literature that total color difference (ΔE) of samples are more
 209 useful for explain materials surface color changes rather than other CIE L^* , a^* , b^* properties
 210 [23]. The highest total color difference value of 8.15 was observed in the control sample
 211 (DE0) while the lowest in DE6 sample (0.63). It was also found that the highest whiteness
 212 color value of -35.48 (in metric) and the corresponding increase in the yellowness color
 213 value of 7.03 (in metric) were found in the DE0 board as well.

214 **TABLE 5** The surface color properties of experimental panels

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Board codes	ΔL	Δa	Δb	ΔE	CIE Whiteness	E313 Yellowness
DE0	-7,19	1,55	3,51	8,15	-35,48	7,03
DE1	-2,78	0,48	0,3	2,84	-8,09	1,01
DE2	1,26	-0,35	1,17	1,75	-3,48	1,56
DE3	-1,12	-0,16	0,8	1,39	-6,9	1,48
DE4	0,17	1,81	-1,46	2,33	8,79	-2,42
DE5	0,98	-0,44	1,27	1,67	-5,13	1,85
DE6	0,47	-0,39	-0,15	0,63	1,91	-0,38

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 218 The comparative Fourier transform infrared spectroscopy (FTIR) analysis of DE0 and DE5
 219 boards are shown in Fig. 5. Generally, bands in the range of $1500-1610\text{ cm}^{-1}$ are considered

220 as a characteristic peak for lignin components and composed of C=O and COO-symmetric
 221 tension vibrations in aromatic rings of lignin structure [14, 24]. However, the bands in the
 222 range of 1360-1380 cm^{-1} were generally showing C-H degradation in polysaccharides. The
 223 change in the bands at 1230-1270 cm^{-1} was reported to explain the vibration in the guayacil
 224 ring with CO groups in lignin and hemicellulose. Although some chemical groups could be
 225 modified under the water/gypsum environment that might be **deteriorated** to some extent
 226 (alkaline environment). In this sense, some bands are modified to some extent but all these
 227 groups observed on the surface of boards.
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Comment [U1]:

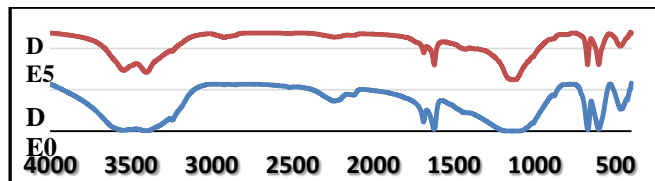


FIG. 5 The FTIR spectra of boards

229 TGA (Thermal Gravimetric Analyzer) analysis based on temperature-time variables at
 230 range of 25-900°C is shown in Fig. 6. The TGA thermographs has divided four different
 231 regions as; heating zone (Tb); (the water assumed to remove) up to 120 °C; cell wall
 232 degradation zone (Tm1); above 120 to 370°C; completely break down zone (Tm2); cell wall
 233 organic constituents completely break down up to 700°C; non-organics degraded zone (Ts)
 234 up to 900°C, on-organics have degraded and char residues obtained. In this approach, the
 235 mass loss of in that zones were found to be 2.5, 27.7, 49 and 55% for DE5 sample,
 236 respectively.
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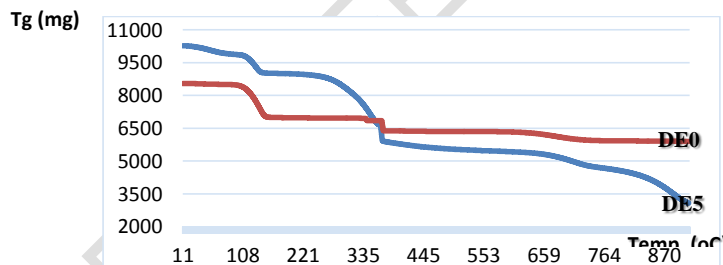


FIG. 6 The TGA micrographs of experimental panels

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 246 According to the TS EN-ISO 11925-2 standard, the flame spreading characteristic of the
 247 boards was conducted. However, the flame spreading pattern of all test boards produced by
 248 adding wood/rice straw-gypsum based boards show that the flame did not reach the
 249 threshold limit of 150 mm. This is a well indication of boards that could be classified as class
 250 A1 (non-flammable material).

251 For determining heat insulation properties, the temperature values passed to the back
 252 surfaces were measured in accordance with DIN 4102 for 30 seconds intervals and for a
 253 total of 300 seconds. The measured values were shown in Table 6. It has been observed
 254 that the addition of rice straw and wood particles to the gypsum structure has a positive
 255 effect on the heat transfer properties. It was measured as 39.1°C in the DE6 panel. When
 256 Table 6 is carefully examined, the addition of rice straw has improving effects on heat
 257 insulation properties of boards. However, the lowest mass loss was also measured as 2.01%

258 on the DE6 boards that produced with the highest rice straw ratio (60:40, rice straw/wood
 259 chips by weight).

260
 261

TABLE 6 The heat insulation properties of boards

	0 (sec.)	60 (sec.)	120 (sec.)	180 (sec.)	240 (sec.)	300 (sec.)	Total Mass loss (%)
DE0	20.2	20.2	24.3	41.9	58.8	66.0	4.15
DE1	20.0	22.7	32.4	45.1	52.0	62.9	3.90
DE2	12.9	15.2	16.3	20.5	30.4	40.9	3.04
DE3	14.2	15.3	23.1	35.0	45.3	56.1	6.21
DE4	10.8	12.9	14.6	19.3	28.7	40.3	2.66
DE5	13.8	14.4	16.0	25.6	32.5	45.3	2.65
DE6	11.8	12.1	15.4	25.1	34.6	39.1	2.01

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4. CONCLUSIONS

In this study, the fundamental knowledge and approaches for producing gypsum based boards from wood/rice straw was investigated. Thus could help researchers to this area gain the understanding and to make meaningful contributions to this field of study. However, it is clear that in order to be an composite panel has efficient mechanical and technological properties, there must be a hydrophobic substances added to mixture for improvement thickness swelling properties in water. Moreover, although the addition of rice straw to the wood/gypsum mixture adversely affected the strength properties negatively, with using some longer fibers may improve the strengths of panels. On the other hand, rice straw in wood chip/gypsum mixture helps to improve heat resistance (insulation) properties some level. It was also realized that the addition of rice straw to wood/gypsum mixture effects on extending hardening time. It is probably gypsum-rice straw interaction that could not effectively wet and penetrate the rice straw surface due to the hydrophobic wax and inorganic silica on the outer surface of rice straw.

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