

**PROPERTIES OF GYPSUM BOARDS MADE OF
MIXTURES OF WOOD AND RICE STRAW**

10
11
12
13
14
15
16
17
18
19
20
21

ABSTRACT

Aims: It was investigated to produce gypsum-based experimental composite panels with red pine wood/rice straw particles in the mixture up to 60:40 (ratio) (w/w) in gypsum-water mixture. In this case, the fillers (additives) could be observed more closely.

Methodology: The red pine wood chips and the rice straw (stalks) have been turned into suitable particle dimensions. The experimental boards were cut to determine the IB (Internal bond), MOE–MOR (Modulus of Elasticity and Rupture), and TS (thickness swelling after 24 hours immersion in water). A standard flame combustion test system was conducted according to TS EN-ISO 11925-2. For surface chemical analyses, FTIR was used to evaluate the chemical groups present in the board surface. The thermogravimetric analysis (TGA) was conducted for measuring changes in boards as a function of increasing temperature. The natural weathering tests were conducted that were exposed to outdoor for two months then color and surface hardness tests conducted for determining property changes.

Results: The rice straw had negative impact on thickness swelling (TS) properties of boards in water. The highest TS value of 47.66% was observed in the board that produced from 60:40 (ratio) (w/w) wood/rice straw mixture (DE4). However, the addition of rice straw to the wood/gypsum mixture has a lowering effect on the internal bond (IB) and bending strength (MOR) properties of experimental boards some level. The maximum IB strength of 0.06 N/mm² and MOR of 2.77 N/mm² found control sample (DE0). However, the highest MOE value of 553 N/mm² was calculated on the DE4 board, which was produced by adding 40% rice straw to the wood/gypsum mixture. The addition of rice straw and wood particles to the gypsum structure has a positive effect on the heat transfer properties.

Conclusion: It is clear that the addition of rice straw to the wood/gypsum mixture adversely affected the strength properties negatively. However, rice straw in wood chip/gypsum mixture helps to improve heat resistance (insulation) properties of panels at some level. Moreover, the addition of rice straw to wood/gypsum mixture effects on extending hardening time.

Keywords: Rice straw, gypsum board, red pine, strength properties, heat insulation

1. INTRODUCTION

Wood has been important raw material sources for housing, energy and decorative purposes. However, in modern times it has become utilized in the fabrication of different products such as paper products, composite panels, furniture and some chemicals [1, 2]. Due to the excessive use of wood, natural forests have become depleted and of scarcity value. The consumers have also become more aware of the importance of preservation and destruction of the natural forests. Thereby, other alternatives have been studied throughout the world such as agricultural residues or wastes, forest residues, low value woody materials, non-wood materials (annual plants), etc. have been found to be useful as added

22 products instead of wood [3-5]. Moreover, there are numerous literature information for
23 utilization of non-wood sources into processing of products [6-11]. The chemical and
24 physical information on those raw materials and processing into composite manufacturing
25 could be found elsewhere [3, 8, 9].
26

27 Rice stalk or straw is one of the abundant lignocellulosic waste materials in the world. It was
28 stated that 709.2 million tons of wheat straw and 673.3 million tons of rice stalks were
29 exposed worldwide and that large amount of lignocellulosic raw material could be used in the
30 production of composite panels [4]. In more recent study, it was proposed that rice is the
31 third most important grain crop in the world behind wheat and corn. According to FAO
32 statistics, world annual rice production in 2007 was about 650 million tons while every
33 kilogram of grain harvested is accompanied by production of 1–1.5 kg of the straw [12].
34

35 Amini and his group (2018) proposed modified corn starch with urea formaldehyde resin
36 could have a potential to be used as a binder to produce particleboard panels with accepted
37 properties [13]. In recent study, the urea-formaldehyde glue was used as a binder for
38 producing cotton waste-based panels with red pine chips and fibers, separately. It was
39 concluded that in some preparation conditions, it is possible to produce particle- and
40 fiberboards with cotton-based waste materials at acceptable level [14].
41

42 However, gypsum is one of the oldest construction materials throughout human beings. The
43 gypsum based construction and ornamental materials were found ancient civilizations (i.e.
44 Sumerian, Seljuk, Ottoman Aztec, Egyptian, Greek and Roman so on). It was used
45 intensively in Renaissance architecture period in Europe due to its easy shape in interior and
46 exterior spaces by architects and painters [15].
47

48 In this study, gypsum-based experimental composite panels was produced with red pine
49 wood/rice straw particles in the mixture up to 60:40 (ratio) (w/w) in gypsum-water mixture.
50 Thus, it is possible to produce gypsum-based experimental panels by selecting the most
51 suitable processing conditions.
52

53 2. MATERIAL AND METHODS

54

55 The red pine wood chips were supplied from a local timber company where processing log to
56 timber, Isparta-Turkey. The rice straw (stalks) was supplied from Can-Biga region of Turkey.
57 Both raw materials have been carefully cleaned from dust, bark and other substances then
58 turned into particles using scissors and screened to suitable particle dimensions. The 10-50
59 mm particles were utilized for mixing with gypsum/water. They were then dried at
60 atmospheric conditions until at least a 10-12% moisture content was obtained.
61

62 The commercial grade perlite plaster type Gypsum, used as binder agent, supplied by a
63 local company, Isparta Turkey. After manufacturing, the experimental boards, they were
64 conditioned at 20 °C and 65% relative humidity. The detailed description of cellulosic raw
65 materials, gypsum with their specifications, and manufacturing process could be found
66 elsewhere [15].
67

68 A total of 14 boards (two for each condition) were made. The experimental procedure for
69 manufacturing experimental particle boards as follows:

- 70 • Press temperature (°C): Ambient temperature
- 71 • Pressing time (day): up to 14
- 72 • Press pressure (N/mm²): 0.1-1.0
- 73 • Wood particles/rice stalk ratio (w/w,%): 100-40/0-60
- 74 • Board dimensions (mm): 400x400x10 cm.

75 • Target density (gr/cm^{-3}): 0.75 (± 0.1).
76

77 It is important to note that the compatibility of gypsum, red pine particles and rice straw are
78 important but not considered in this study. However, some certain chemicals may also be
79 used to shorten the curing time and improve compatibility of these substances into gypsum.
80 Therefore, only the pure effects of wood/gypsum/rice straw compatibility are considered.
81

82 After reaching full strength at ambient temperature, the experimental boards were
83 conditioned at 20 °C and 6-8 % relative humidity and samples were cut to determine the IB
84 (Internal bond), MOE–MOR (Modulus of Elasticity and Rupture), TS (thickness swelling after
85 24 hours immersion in water), in accordance with TS EN 310 (1999), TS EN 319 (1999) and
86 TS EN 317 (1999), ASTM D 1037, respectively [16-18].
87

88 A standard flame combustion test system was conducted according to TS EN-ISO 11925-
89 2. A visual observation of the sample was made either or not the flame spreads in the
90 vertical direction more than 150 mm above from the flame application point [19-22]. For
91 surface chemical analyses, FTIR spectrophotometer (A Shimadzu (IR Prestige-21) was used
92 to evaluate the chemical groups present in surfaces. For thermogravimetric analysis (TGA),
93 Perkin Elmer SII instrument was utilized for measuring changes as a function of increasing
94 temperature.
95

96 The natural weathering tests were conducted on 50x50x10 mm samples were exposed to
97 outdoor for two months then color and surface hardness tests conducted for determining
98 property changes. The total color differences (ΔE) of the samples were measured by X-Rite
99 SP 68 Spectrophotometer using CIE L*, a*, b* standards (1976). The surface hardness
100 properties of both control and weathered samples were measured with a Shore D hardness
101 tester, according to test method of ASTM D2240 standard [23]. The board's code numbers
102 (wood chip and rice straw ratios) with constant gypsum content (800 gr) at various
103 proportions are given in Table 1.
104

105 **Table 1.** The proportions and code numbers of gypsum boards

Board code	Wood (gr)	Rice straw (gr)	Wood (%)	Rice straw (%)
DE0	1000	0	100	0
DE1	900	100	90	10
DE2	800	200	80	20
DE3	700	300	70	30
DE4	600	400	60	40
DE5	500	500	50	50
DE6	400	600	40	60

106

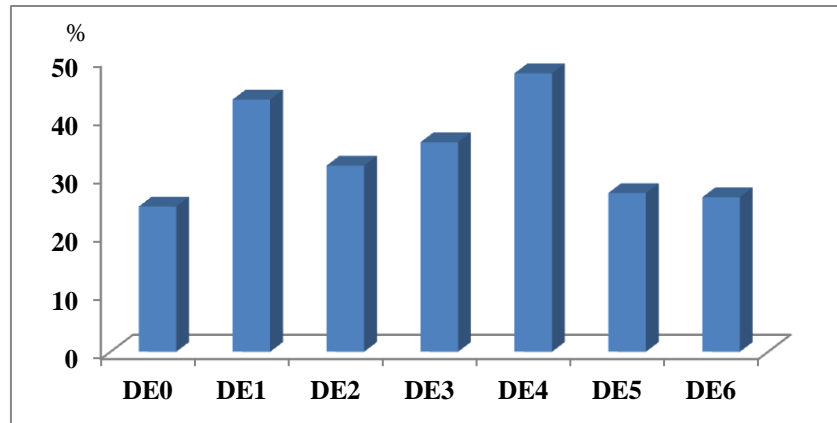
107

108 3. RESULTS AND DISCUSSION

109

110 The thickness swelling properties of experimental boards after immersing in water are shown
111 in Figure 1. It was realized that the lowest thickness swelling of 24.85% was observed in the
112 panels produced from only the mixture of wood/gypsum (DE0) (no rice straw added). The
113 addition of rice straw to the mixture had adversely affects the thickness swelling properties.
114 The highest thickness swelling value of 47.66% found at 60:40 wood/rice straw (w/w)
115 mixture (DE4) condition. Interestingly, it was found that the panels include rice straw was
116 equal and/or higher than the wood chips (DE5 and DE6 boards), the thickness swelling

117 values of 27.18 and 26.45% were found that only marginally similar to control sample (DE0),
 118 respectively.
 119



120 **Fig. 1** Thickness swelling properties of experimental boards in water
 121
 122

120
 121
 122
 123
 124
 125
 126
 127
 128
 129

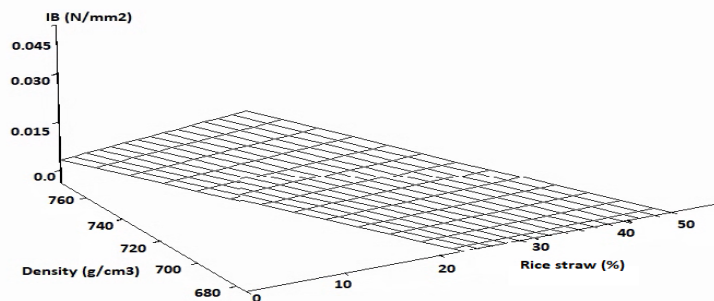
The comparative internal bond (IB) strength properties of experimental boards are shown in Table 2. The test boards produced from wood/rice straw-gypsum boards were lower than those of the board produced only with wood/gypsum mixture (DE0). That is, the addition of rice straw to the wood/gypsum mixture has a negative effect on the IB strengths in all conditions. The maximum IB strength was calculated as 0.06 N/mm² for control sample.

130 **Table 2** The IB strength properties of gypsum boards

Board code	Density (kg/m ³)	Internal bond (IB) (N/mm ²)	Difference from control (DE0) (%)
DE0	709.99	0.06	0.0
DE1	747.94	0.012	-80.0
DE2	717.94	0.014	-76.7
DE3	719.31	0.015	-75.0
DE4	705.89	0.013	-78.3
DE5	699.70	0.012	-80.0
DE6	697.48	0.011	-81.7

130
 131
 132
 133

The combined effects of panel density and rice straw additive level on IB properties shown in Fig. 2. As seen, all rice straw addition negatively effects on IB properties some level. However, increasing panel's density had not much impact on IB of boards.



134

135
136
137
138
139
140
141
142
143
144
145
146
147
148
149
150
151
152
153
154
155
156
157
158

Fig. 2 IB properties of experimental boards.

The bending strength values of the experimental panels (MOR) produced with various proportion additions to rice straw (D1 to D6) was found to be lower than those produced from only wood/gypsum mixture (DE0) (Table 3). This is obviously important in that the introduction of rice straw into the wood/gypsum mixture has the reducing effects on bending strength properties. However, the lowest MOR value was calculated as 0.97 N/mm² in the DE3 panel (70:30; wood chip/rice straw mixture).

The elastic modulus characteristics (MOE) of the boards are also show similar trend (Table 3). The highest MOE value of 553 N/mm² was calculated on the DE4 board, which was produced by adding 40% rice straw to the wood/gypsum mixture. It was clearly seen that the elastic modulus values of all boards produced by the addition of rice straw into wood/gypsum mixture were improved up to 60:40 wood/rice straw level (w/w), beyond this level, the MOE values of experimental panels significantly reduced. In this sense, except a few conditions, the similar situations were also observed for internal bond strength (IB) and bending strength (MOR) properties. It could be summarize that the compatibility of rice straw with gypsum is low and should be useful only in controlled conditions.

The Duncan's multiple range test results also showed that the rice straw and wood chips ratio had some statistically different MOR values that it was in the two groups for MOR while no statistically difference in MOE values.

Table 3 Bending strength and modulus of elasticity of experimental panels

Board Code	MOR (N/mm ²)	Difference from control (%)	MOE (N/mm ²)	Difference from control (%)
DE0	2.77 (B)	0.0	445	0.0
DE1	1.21 (A)	-56.3	113	-74.6
DE2	1.22 (A)	-55.9	192	-56.9
DE3	0.97 (A)	-64.5	443	-0.23
DE4	1.07 (A)	-61.4	553	24.3
DE5	1.16 (A)	-58.1	360	-19.1
DE6	2.30 (B)	-16.9	138	-68.9

159
160
161
162
163
164
165
166

*Groups with the same letters in each column indicate that there is no statistical difference (P< 0.05) between the samples according to the Duncan's multiple range test.

The combined effects of both panels density and rice straw ratio impact on bending strength properties of experimental boards are shown in Figure 3. It could be seen that increasing rice straw ratio and panel's density has only marginally effects on panel's MOR values.

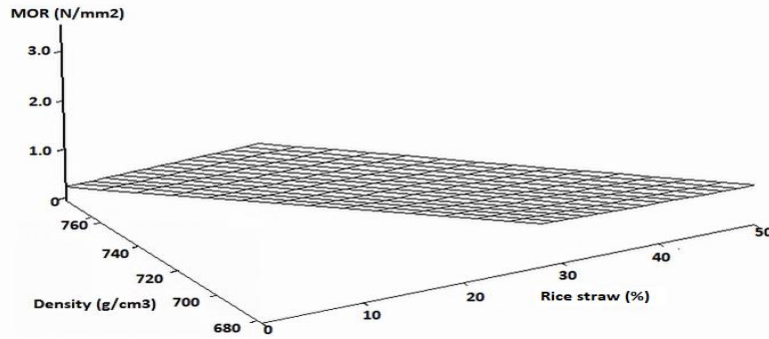


Fig. 3 Panel density and rice straw ratio effects on bending strength of experimental boards

167
168
169
170
171
172
173
174
175
176
177
178
179
180
181
182
183
184
185
186
187

The comparative surface hardness values (Shore D) of the test panels are given in Table 4. The highest Shore D value of 44 (metric) was observed on the DE0 board while the lowest value of 22 found for DE5 board produced from the mixture of 50:50 wood/rice straw. In general, it has understood that the hardness values of the boards produced with the increase in rice straw or the decrease in the wood ratio (at fixed the gypsum ratio) are affected negatively on hardness properties. However, an interesting situation was encountered that the hardness values of the boards kept under external atmospheric conditions were found to decrease less than the DE0 sample. The lowest hardness value reduction in the boards that were kept under external atmospheric conditions was calculated as 3.2% in DE3 and 4.3% in DE1 type boards, respectively. The increase in the ratio of rice straw in the mixture adversely affects the hardness values, but it is important to ensure that the hardness properties of the panels against external atmospheric conditions remain at a lower trend than control sample (DE0).

However, according to Duncan's multiple range test result, rice straw and wood chips ratio had some statistically different hardness values that it was in the six statistically different groups for this study.

Table 4. Surface hardness properties of boards

Board code	Hardness (metric)	Diffrence from control (DE0) (%)	After weathering hardness (metric)	Changes (%)
DE0	44 (D)	0,0	33	-25
DE1	45 (E)	2.2	43	-4.4
DE2	32 (BC)	-27.2	27	-15.6
DE3	31 (CD)	-29.9	30	-3.2
DE4	23 (A)	-47.8	21	-8.7
DE5	22 (A)	-50.0	20	-9.1
DE6	26 (AB)	-40.9	25	-3.8

188
189
190
191
192
193
194

*Groups with the same letters in each column indicate that there is no statistical difference ($P < 0.05$) between the samples according to the Duncan's multiple range test.

The effects of wood and rice straw ratio on both control and weathered experimental panels are shown in Figure 4. It was realized that the similar trend was found for both panels that increasing rice stalk ratio or (decreasing wood ratio) negatively effects on experimental panels.

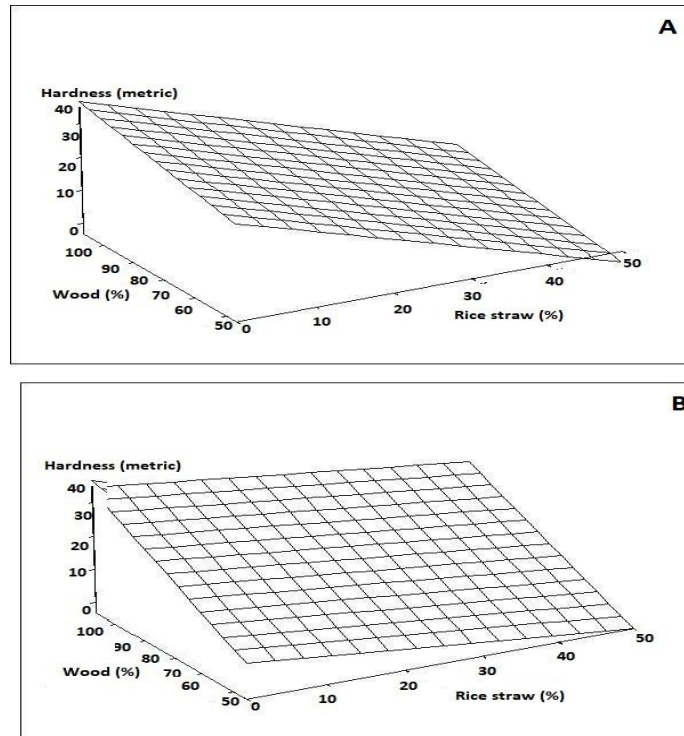


Fig. 4 Hardness properties of boards (A: Control samples, B: Weathered samples)

195
196
197
198
199
200
201
202
203
204
205
206
207

The comparative surface optical (color) properties of boards are shown in Table 5. In general, it was proposed in literature that total color difference (ΔE) of samples are more useful for explain materials surface color changes rather than other CIE L^* , a^* , b^* parameters [23]. The highest ΔE value of 8.15 was observed in the control sample (DE0) while the lowest in DE6 sample (0.63). It was also found that the highest whiteness color value of -35.48 (in metric) and the corresponding increase in the yellowness color value of 7.03 (in metric) were found in the DE0 board as well.

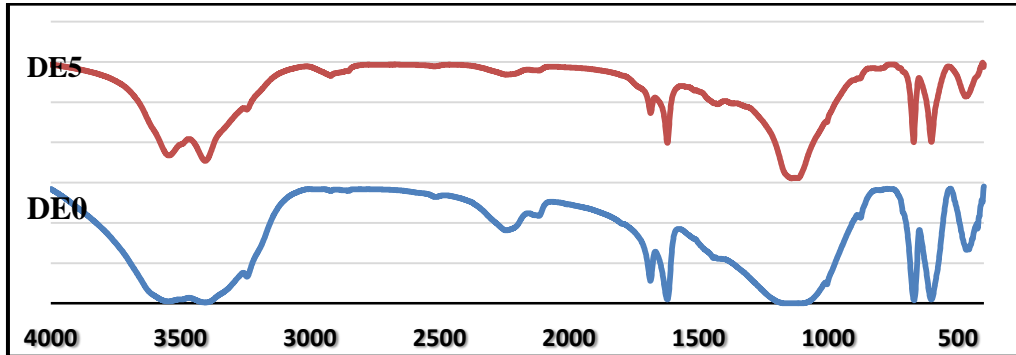
Table 5 The surface color properties of experimental panels

Board codes	ΔL	Δa	Δb	ΔE	CIE Whiteness	E313 Yellowness
DE0	-7,19	1,55	3,51	8,15	-35,48	7,03
DE1	-2,78	0,48	0,3	2,84	-8,09	1,01
DE2	1,26	-0,35	1,17	1,75	-3,48	1,56
DE3	-1,12	-0,16	0,8	1,39	-6,9	1,48
DE4	0,17	1,81	-1,46	2,33	8,79	-2,42
DE5	0,98	-0,44	1,27	1,67	-5,13	1,85
DE6	0,47	-0,39	-0,15	0,63	1,91	-0,38

208
209
210
211
212

The comparative Fourier Transform Infrared Spectroscopy (FTIR) analysis of DE0 and DE5 boards are shown in Fig. 5. Generally, bands in the range of $1500-1610 \text{ cm}^{-1}$ are considered as a characteristic peak for lignin components and composed of C=O and COO-symmetric tension vibrations in aromatic rings of lignin structure [15, 25]. However, the

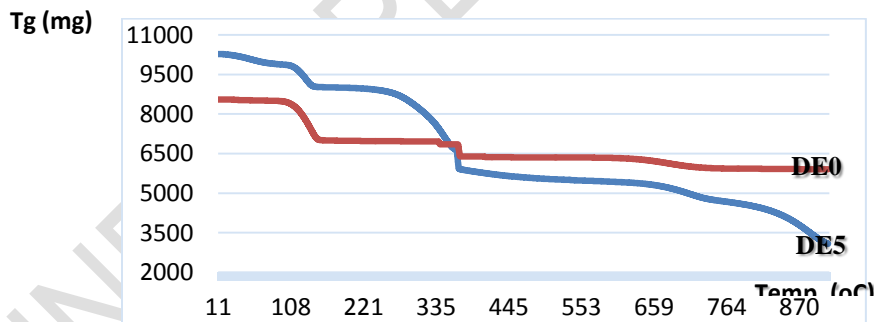
213 bands in the range of 1360-1380 cm^{-1} were generally showing C-H degradation in
 214 polysaccharides. The change in the bands at 1230-1270 cm^{-1} was reported to explain the
 215 vibration in the guayacil ring with CO groups in lignin and hemicellulose. Although some
 216 chemical groups could be modified under the water/gypsum environment that might be
 217 **deteriorated** to some extent (alkaline environment). In this sense, some bands are modified
 218 to some extent but all these groups observed on the surface of boards.
 219



220 **Fig. 5** The FTIR spectra of boards

221
 222
 223
 224
 225
 226
 227
 228
 229
 230
 231
 232

TGA (Thermal Gravimetric Analyzer) analysis based on temperature-time variables at
 range of 25-900°C is shown in Fig. 6. The TGA thermographs has divided four different
 regions as; heating zone (T_b); (the water assumed to remove) up to 120 °C; cell wall
 degradation zone (T_{m1}); above 120 to 370°C; completely break down zone (T_{m2}); cell wall
 organic constituents completely break down up to 700°C; non-organics degraded zone (T_s)
 up to 900°C, on-organics have degraded and char residues obtained. In this approach, the
 mass loss of in that zones were found to be 2.5, 27.7, 49 and 55% for DE5 sample,
 respectively.



233 **Fig. 6** The TGA micrographs of experimental panels

234
 235
 236
 237
 238
 239
 240
 241
 242
 243
 244
 245
 246

According to the TS EN-ISO 11925-2 standard, the flame spreading characteristic of the
 boards was conducted. However, the flame spreading pattern of all test boards produced by
 adding wood/rice straw-gypsum based boards show that the flame did not reach the
 threshold limit of 150 mm. This is a well indication of boards that could be classified as class
 A1 (non-flammable material).

For determining heat insulation properties, the temperature values passed to the back
 surfaces were measured in accordance with DIN 4102 for 30 seconds intervals and for a
 total of 300 seconds. The measured values were shown in Table 6. It has been observed
 that the addition of rice straw and wood particles to the gypsum structure has a positive
 effect on the heat transfer properties. It was measured as 39.1°C in the DE6 panel. When

247 Table 6 is carefully examined, the addition of rice straw has improving effects on heat
 248 insulation properties of boards. However, the lowest mass loss was also measured as 2.01%
 249 on the DE6 boards that produced with the highest rice straw ratio (60:40, rice straw/wood
 250 chips by weight).

251
 252

Table 6 The heat insulation properties of boards

	0 (sec.)	60 (sec.)	120 (sec.)	180 (sec.)	240 (sec.)	300 (sec.)	Total Mass loss (%)
DE0	20.2	20.2	24.3	41.9	58.8	66.0	4.15
DE1	20.0	22.7	32.4	45.1	52.0	62.9	3.90
DE2	12.9	15.2	16.3	20.5	30.4	40.9	3.04
DE3	14.2	15.3	23.1	35.0	45.3	56.1	6.21
DE4	10.8	12.9	14.6	19.3	28.7	40.3	2.66
DE5	13.8	14.4	16.0	25.6	32.5	45.3	2.65
DE6	11.8	12.1	15.4	25.1	34.6	39.1	2.01

253
 254
 255

4. CONCLUSIONS

256 In this study, the fundamental knowledge and approaches for producing gypsum based boards
 257 from wood/rice straw was investigated. Thus could help researchers to this area gain the
 258 understanding and to make meaningful contributions to this field of study. However, it is clear
 259 that in order to be an composite panel has efficient mechanical and technological properties,
 260 there must be a hydrophobic substances added to mixture for improvement thickness swelling
 261 properties in water. Moreover, although the addition of rice straw to the wood/gypsum mixture
 262 adversely affected the strength properties negatively, with using some longer fibers may
 263 improve the strengths of panels. On the other hand, rice straw in wood chip/gypsum mixture
 264 helps to improve heat resistance (insulation) properties some level. It was also realized that
 265 the addition of rice straw to wood/gypsum mixture effects on extending hardening time. It is
 266 probably gypsum-rice straw interaction that could not effectively wet and penetrate the rice
 267 straw surface due to the hydrophobic wax and inorganic silica on the outer surface of rice
 268 straw.

269
 270

REFERENCES

271
 272
 273
 274
 275
 276
 277
 278
 279
 280
 281
 282
 283
 284
 285
 286

1. Forest Products Laboratory. Wood Handbook-Wood as an engineering material, *General Technical Report FPL-GTR-190*, Madison, WI, 508p. 2010.
2. Janick, J., Schery, R.W., Woods, F.W. and Ruttan, V.W. Plant Science: An Introduction to world crops, (3rd ed.). *W. H. Freeman & Co.* San Francisco, 868p. 1981.
3. Rowell, R.M. Opportunities for composites from agro-based resources, In: Paper and composites from agro based resources, R.M. Rowell, R.A. Young, J.K. Rowell, (Eds), CRC Press Inc, Boca Raton, FL. 1996.249-300pp.
4. Mantanis G., Nakos P., Berns J. and L. Rigal. Turning agricultural straw residues into value-added composite products: A new environmentally friendly technology. In: Proc. of the 5th International Conference on Environmental Pollution, Aug. 28-31, 2000, *Aristotelian University*, Thessaloniki, Greece, 840-848 pp.
5. Alma, M.H., Kalaycıoğlu, H., Bektaş, I. and Tutuş, A. Properties of cotton carpel based particleboards, *Ind. Crops & Products*, 2005, 22 (2): 141-149.
6. Batalla, L., Nunez, A., J. and Marcovich, N., E., Particleboards from Peanut-shell flour, *J. Appl. Polymer Sci.*, 2005, 97(3):916-923.

- 287 7. Ndazi, B., Tesha, J. V. and Bisanda E.T.N. Some opportunities and challenges of
288 producing bio-composites from non-wood residues, *J. Mater Sci.*, 2006, 41, 6984–6990.
- 289 8. Rials, G. T. and Wolcott, M.P. Physical and mechanical properties of agro-based fibers,
290 In: Paper and composites from agro based resources, Rowell, R.M., Young, R.A., Rowell,
291 J.K. (Eds), *CRC Press Inc*, Boca Raton, Florida, 63-81 pp. 1997.
- 292 9. Youngquist, J.A., English, B.E., Scharmer, R.C., Chow, P. and Shook, S.R. Literature
293 review on use of nonwood plant fibers for building materials and panels, USDA Forest
294 Service, *General Technical Report, FPL-GTR 80*, Madison, WI. 1994.
- 295 10. Youngquist, J.A., Krzysik, A. M., Chow, P. and Meimban, R. Properties of composite
296 panels. In: Paper and composites from Agro-based resources, R.M. Rowell, R.A. Young,
297 J.K. Rowell, (Eds), *CRC Press Inc*, Boca Raton, Florida. 1997.
- 298 11. Sahin, H. T., Yavilioglu, I., & Yalcin, O. U. Properties of Composite Panels Produced from
299 Cotton Waste and Red Pine Wood Mixtures. *Journal of Applied Life Sciences*
300 *International*, 2018, 1-9.
- 301 12. Binod, P., Sindhu, R., Singhania, R. R., Vikram, S., Devi, L., Nagalakshmi, S., ... &
302 Pandey, A. Bioethanol production from rice straw: an overview. *Bioresource technology*,
303 2010, 101(13), 4767-4774.
- 304 13. Amini, M.H.M., Hashim, R., Sulaiman, N.S., Mohamed, M., Masri, M.N., Sobri, S.A.,
305 Ibrahim, N.I. Study on Dimensional Stability of Particleboard Made Using
306 Glutardialdehyde Modified Corn Starch as the Binder at Various Relative Humidity,
307 *International Journal of Engineering & Technology*, 2018, 7(2.15): 19-22.
- 308 14. Yavilioglu, I. Investigation properties of boards made from mixtures of cotton waste and
309 red pine wood, Süleyman Demirel Üniversitesi, Fen Bilimleri Enstitüsü, Yüksek Lisans
310 Tezi, 2017, 86s, Isparta. (Turkish abstract in English)
- 311 15. Demir, I. Investigation of the technological properties of gypsum composites produced
312 from some cellulosic based secondary fiber sources, Süleyman Demirel Üniversitesi Fen
313 Bilimleri Enstitüsü, MSc. Thesis, 2019, 113 p., Isparta. (Turkish abstract in English)
- 314 16. TS EN 310. Wood- Based panels- Determination of modulus of elasticity in bending and
315 of bending strength, 1999, *TSE*, Ankara.
- 316 17. TS EN 317. Particleboards and fibreboards- Determination of swelling in thickness after
317 immersion in water, 1999, *TSE*, Ankara.
- 318 18. TS EN 319. Particleboards and fibreboards- Determination of tensile strength
319 perpendicular to the plane of the board, (Turkish Standard), 1999, *TSE*, Ankara.
- 320 19. TS EN 13501-1. Fire classification of construction products and building elements – Part
321 1: Classification using test data from reaction to fire tests, (Turkish Standard), 2003, *TSE*,
322 Ankara.
- 323 20. TS EN 11925-2. Reaction to fire tests - Ignitability of building products subjected to direct
324 impingement of flame - Part 2: Single-flame source test, Turkish Standards Institution,
325 2002, Ankara.
- 326 21. ASTM-C 1113-09 Standard Test Method for Thermal Conductivity of Refractories by Hot
327 Wire (Platinum Resistance Thermometer Technique), 2013.
- 328 22. TS EN 13501-1. Fire classification of construction products and building elements – Part
329 1: Classification using test data from reaction to fire tests, (Turkish Standard), 2003, *TSE*,
330 Ankara.
- 331 23. ASTM D2240-15e1, Standard Test Method for Rubber Property—Durometer Hardness,
332 2015, ASTM International, West Conshohocken,
- 333 24. Sahin, H.T., Arslan, M.B., Korkut, S., Kus Sahin, C. Colour changes of heat-treated
334 woods of red-bud maple, European hophornbeam and oak. *Color Research &*
335 *Application*, 2011, 36(6), 462-466.
- 336 25. Pandey, K. K. A Note On The Influence Of Extractives On The Photo-Discoloration And
337 Photo-Degradation Of Wood. *Polymer degradation and stability*, 2005, 87(2), 375-379