



39 metal. Although weld metal properties are primarily controlled by the consumable composition  
40 of the shielding gas which can directly influence the strength and ductility of a weld. Its  
41 paramount to understand the statistical influence of process parameters in mild steel cladding  
42 weld bead geometry.

43 This study investigates the application of statistics and to analyze the influence of cladding  
44 weld metal geometry on mild steel using the response surface method with the application of  
45 TIG welding method. Therefore, the main objective of the study is to determine and to evaluate  
46 the statistical solutions and its influences of the impact strength in mild steel cladding weld metal  
47 bead geometry.

## 48 **2. PROCESSES OF WELDING**

49 These processes use a welding power supply to create and maintain an electric arc between an  
50 electrode and the base material to melt metals at the welding point. They can use either direct  
51 current (DC) or alternating current (AC), and consumable or non-consumable electrodes. The  
52 welding region is sometimes protected by some type of inert or semi-inert gas, known as a  
53 shielding gas, and filler material is sometimes used as well (Lincoln, 2014).

### 54 **2.1 Review of related literature under study**

55 Palani and Murugan (2006), expressed the mechanical and corrosion-resistant properties of the  
56 coated components depend on the geometries of the coated beads, which in turn are controlled by  
57 the process parameters. Therefore, it is essential to study the effect of the process parameters on  
58 the cord geometry to allow effective control of these parameters. The above objective can be  
59 easily achieved by developing equations to predict the dimensions of the weld bead in terms of  
60 process parameters. The models developed were reviewed for their suitability. Confirmation  
61 experiments were also performed and the results show that the developed models can predict the  
62 geometries and the dilution of the beads with reasonable precision. It was observed from the  
63 research that the interactive effect of the parameters of the process in the geometry of the account  
64 is significant and cannot be neglected. Eutimio et al (2013), shows that most of statistical tools  
65 currently applied in the bioprocess area were classified. The main three categories were: fair  
66 comparison of results, mathematical modeling for little studied systems and taking advantage of  
67 large volume of data for enhance robustness and efficiency. However, a chart was constructed

68 for guiding researchers to select the correct statistical technique according to the specific  
69 bioprocess problem.

70 Achebo (2016) describes the process of developing a model that relates the shear stresses in a  
71 gas welded **aluminum** alloy weldment with the corresponding flux constituent elements that  
72 make up the flux composition. The weldments made from the 13 flux compositions were  
73 subjected to evaluation by some professional welders whose judgments about the quality of the  
74 weldments were evaluated by using the rank correlation coefficient method. Stefano et al (2009)  
75 present the results of a research through the design of an experimental technique on the influence  
76 of temperature, the residence time and the pressure of the bar in the resistance to heat sealing of  
77 oriented polypropylene films coated with a thin layer of gelatin. This chemo-metric approach  
78 allowed to achieve a complete understanding of the effect of each independent factor in the two  
79 different responses considered as a measure of the force required to break the link through the  
80 sealed interface.

81 Marko et al (2017), express that the process of laser cladding has become more important  
82 during recent years because of its broad application for cladding, repair or additive  
83 manufacturing. For high quality and reliability of the repaired components, it is necessary to  
84 adjust the weld bead geometry to the specific repair task. The bead geometry influences the  
85 metallurgical bonding and the degree of dilution as well as the formation of defects like pores or  
86 cracks. The results show, the essential effects are detected with a full factorial test plan as well as  
87 with a central composite design. Merely the effect strength could not always be specified  
88 unambiguously. Mastanaiah et al (2014) described the Prediction of weld bead geometry is  
89 always an interesting and challenging research as it involves understanding of complex multi  
90 input and multi output system. The weld bead geometry has a profound impact on the load  
91 bearing capability of a weld joint. The results of investigation suggests the effective thickness of  
92 weld, a geometric parameter of weld bead has the most significant influence on tensile breaking  
93 load of dissimilar weld joint. The observations on bead geometry and the mechanical are  
94 correlated with detailed metallurgical analysis. Xu et al (2014) described the oscillating arc  
95 narrow gap all-position gas metal arc welding process was developed to improve efficiency and  
96 quality in the welding of thick-walled pipes. The developed models were checked for their

97 adequacy and significance by ANOVA, and the effects of wire feed rate, travel speed, dwell  
 98 time, oscillating amplitude and welding position on weld bead dimension were studied. Finally,  
 99 the optimal welding parameters at welding positions of 0° to 180° were obtained by numerical  
 100 optimization using RSM. Nuri et al (2013) study is aimed at obtaining a relationship between the  
 101 values defining bead geometry and the welding parameters and also to select optimum welding  
 102 parameters. The welding process parameters that have the most effect on bead geometry are  
 103 considered and the other parameters are held as constant. Then, the relationship between the  
 104 welding parameters is modeled by using artificial neural network (ANN) and neuro-fuzzy system  
 105 approach. The models developed are compared with regard to accuracy and the appropriate  
 106 welding parameters values can be easily selected when the models improve.

107 **3. EXPERIMENT DESIGN**

108 Design of experiment is a scientific approach of combining input parameters optimally so as to  
 109 optimize a target response and this can be achieved by using computer software like design  
 110 expert. For proper polynomial approximation, experimental designs are used to collect the data.  
 111 There are different types of experimental designs which include central composite design,  
 112 taguchi, D-optimal design, factorial design and latin hyper cube designs.

113 **3.1 Identification of range of input parameters**

114 The key parameters considered in this work are welding current, gas flow rate, welding speed  
 115 and voltage. The range of the process parameters obtained from literature is shown in the table  
 116 below

117 **TABLE 1 Process parameters at low and high levels**

Parameter	Units	Symbol	Low	High
Current	Amp	A	180	240
Gas flow rate	Lit/min	F	10	16
Voltage	Volt	V	18	24
Welding speed	Mm/s	S	90	145

118 Impact testing machine is a machine used for the impact testing analysis. It is used to test the  
 119 impact strength of the materials to determine the energy or strength of the materials at a specific  
 120 location of the material basically at the weldment and other specified locations the researcher

121 wished to determine the strength in that location. It measures the unit of the material strength in  
122 Joules.



**FIG. 1 Impact Testing Setup**

123  
124

125 In the fabrication industry materials standard and specification plays a very vital role in  
126 achieving good weld quality .The welding parameter specification is shown in the table below.

### 127 **3.5 Method of Data Collection**

128 The central composite design matrix was developed using the design expert software, producing  
129 20 experimental runs. The input parameters and output parameters make up the experimental  
130 matrix and the responses recorded from the weld samples was used as the data. The input process  
131 factors are welding current, welding voltage, welding speed and gas flow rate. The output  
132 process response is impact strength of the weldment. The input and output parameters were  
133 analyzed statistically modeled and optimized.

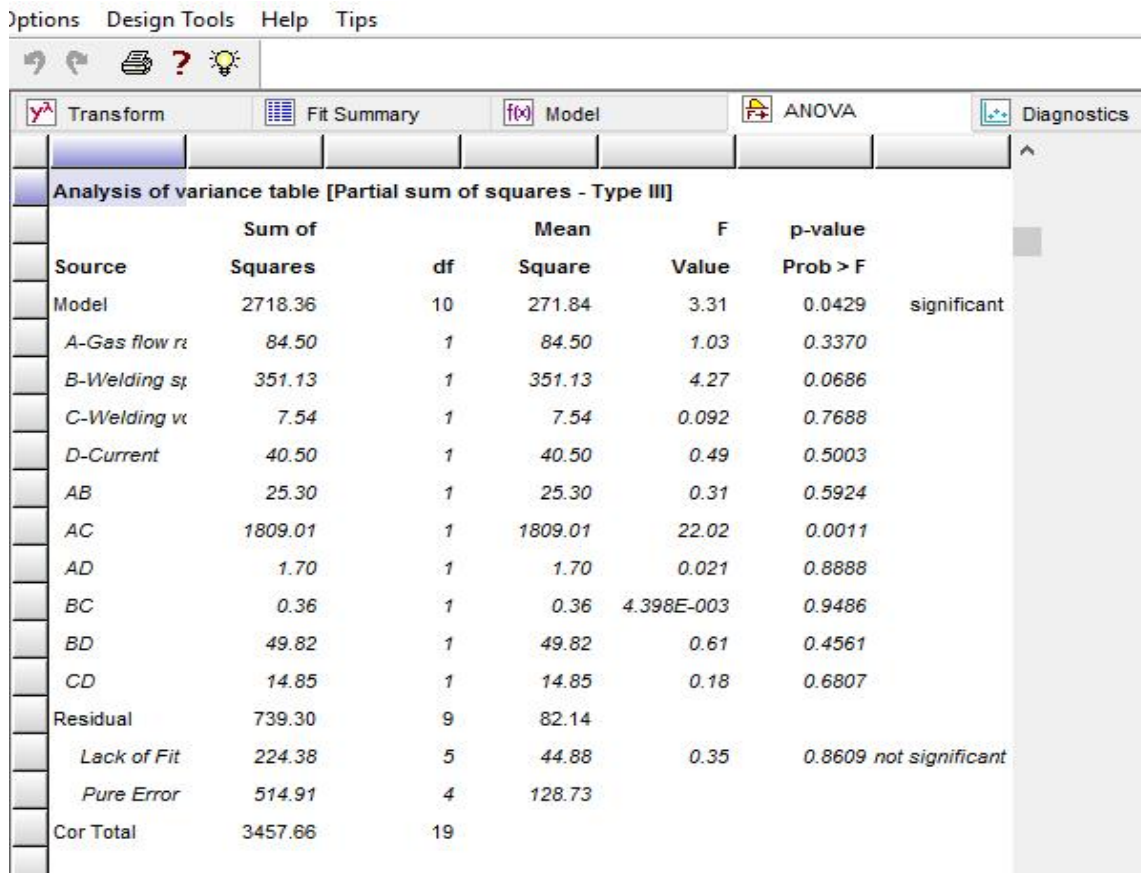
### 134 **3.6 Method of Data Analysis**

135 Response Surface Methodology (RSM) Engineers often search for the conditions that would  
136 investigate the process of interest. RSM is one of the techniques currently in widespread usage to  
137 describe the performance of the welding process and find the statistical investigation of the  
138 responses of interest. RSM is a set of mathematical and statistical techniques that are useful for  
139 modeling and predicting the response of interest affected by several input variables with the aim  
140 of optimizing this response.

## 141 **4. MODELING AND STATISTICAL EVALUATION USING RESPONSE SURFACE** 142 **TECHNIQUE**



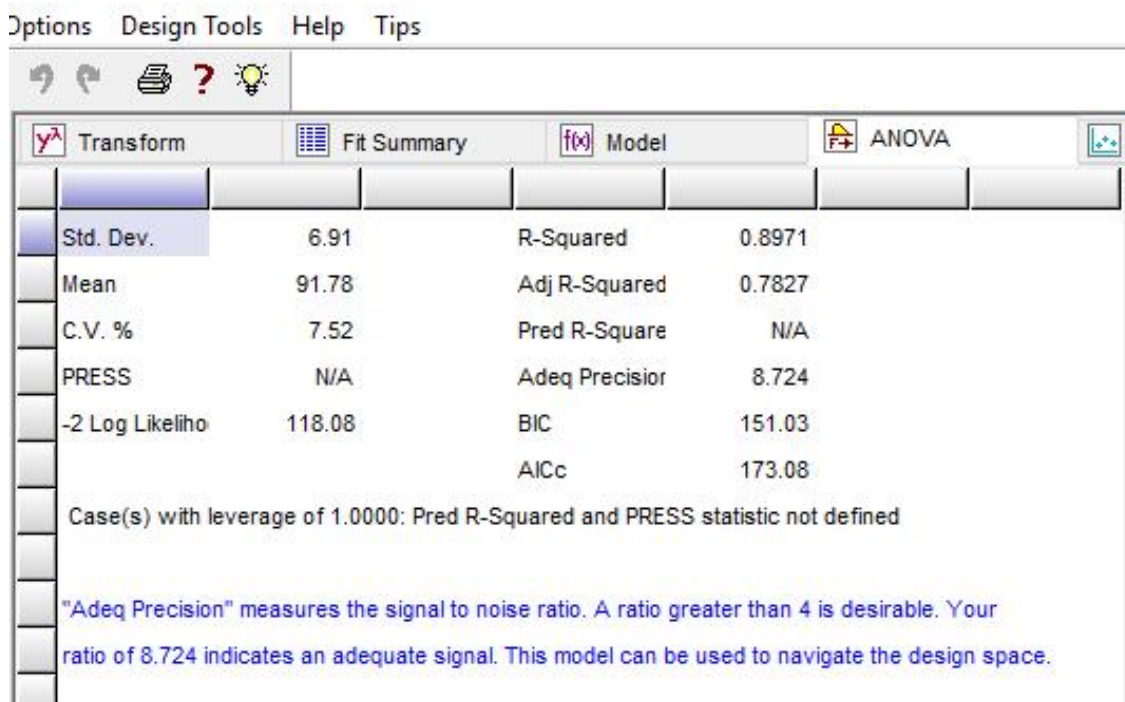
143 In this research, the researcher revealed a mathematical relationship between selected process  
 144 factors, namely; current, speed, gas flow rate and voltage to the response variable. The response  
 145 variable of interest is impact strength of the material.



146 **FIG. 2 ANOVA for validating the model significance to analyze the impact strength**

147 Analysis of the model standard error was employed to assess the suitability of process factor  
 148 and response variables using the central composite design model in response surface to optimize  
 149 the impact strength on the weldment. The computed ANOVA of design responses was presented  
 150 in figure 2. From the results of figure 2, the Model has ten (10) degree of freedom, with the  
 151 model F-value of 3.31 which implies that the model is significant. There is only a 4.29% chance  
 152 that an F-Value this large could occur due to noise. Values of "Prob > F" less than 0.0500  
 153 indicate model terms are significant. In this case A, D, AC are significant model terms. Values  
 154 greater than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of  
 155 0.35 implies the Lack of Fit is not significant relative to the pure error. There is 86.09% chance  
 156

157 that a "Lack of Fit F-value" this large could occur due to noise. Non-significant lack of fit is  
158 good for the model fitness.



159  
160 **FIG. 3 Model summary analysis for validating the model significance on the impact**  
161 **strength**  
162

163 To validate the adequacy of the model based on its ability to maximize the impact strength,  
164 the goodness of fit statistics was presented in figure 3. From the result of figure 3, it was  
165 observed that the "Predicted R-Squared" value of null is obtained. In case(s) where leverage of  
166 1.0000 is obtained, Predicted R-Squared and PRESS statistic are not defined. However, the R-  
167 Squared value of the model is 0.8971 while the Adjusted R-Squared value of the model is  
168 0.7827. "Adequate Precision" measures the signal to noise ratio. A ratio greater than 4 is  
169 desirable. The computed ratio of 8.724 as observed in figure 3 indicates an adequate signal.  
170 This model can be used to navigate the design space. Variance inflation factor (VIF) less than  
171 10.00 calculated for all the terms in the design indicate a significant model in which the variables  
172 are correlated with the response.

Diagnostics Case Statistics									
Run	Actual	Predicted			Internally	Externally		Influence on	
Order	Value	Value	Residual	Leverage	Studentized	Studentized	Cook's	Fitted Value	Standard
					Residual	Residual	Distance	DFBETS	Order
1	80.00	75.42	4.58	0.553	0.991	0.990	0.110	1.101	15
2	75.00	74.54	0.46	0.876	0.190	0.179	0.023	0.477	8
3	110.00	109.54	0.46	0.876	0.190	0.179	0.023	0.477	4
4	90.50	88.68	1.82	0.876	0.748	0.729	0.359	1.935	7
5	112.00	111.54	0.46	0.876	0.190	0.179	0.023	0.477	5
6	72.00	70.18	1.82	0.876	0.748	0.729	0.359	1.935	6
7	70.00	70.00	0.000	1.000					9
8	85.00	90.81	-5.81	0.260	-0.977	-0.974	0.030	-0.577	13
9	90.00	92.92	-2.92	0.053	-0.435	-0.414	0.001	-0.098	18
10	100.00	98.67	1.33	0.553	0.288	0.273	0.009	0.303	12
11	88.50	87.17	1.33	0.553	0.288	0.273	0.009	0.303	11
12	96.00	92.92	3.08	0.053	0.458	0.437	0.001	0.103	19
13	71.50	71.04	0.46	0.876	0.190	0.179	0.023	0.477	2
14	81.00	92.92	-11.92	0.053	-1.774	-2.073	0.016	-0.489	21
15	115.00	110.42	4.58	0.553	0.991	0.990	0.110	1.101	16
16	102.00	92.92	9.08	0.053	1.351	1.426	0.009	0.336	17
17	105.00	103.18	1.82	0.876	0.748	0.729	0.359	1.935	1
18	116.50	114.68	1.82	0.876	0.748	0.729	0.359	1.935	3
19	89.50	92.92	-3.42	0.053	-0.509	-0.487	0.001	-0.115	20
20	86.00	95.04	-9.04	0.260	-1.521	-1.664	0.074	-0.985	14

**FIG. 4 Diagnostics case statistics of the impact strength (J)**

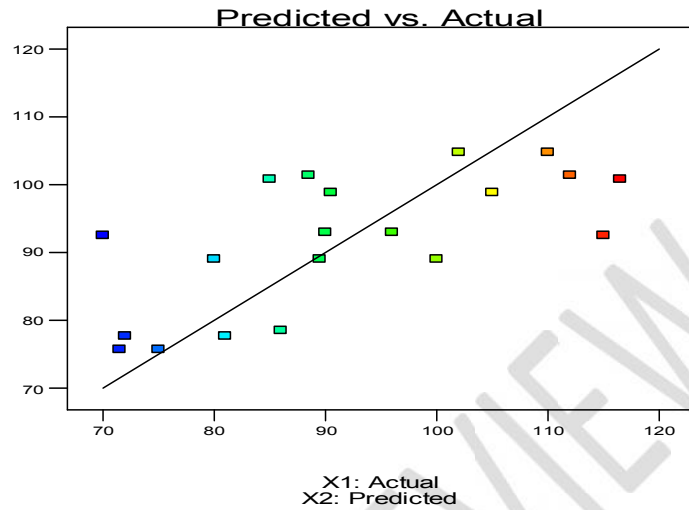
173  
174  
175  
176  
177  
178  
179  
180

The diagnostics case statistics report which shows the observed values of each response variable (impact strength) against their predicted values is presented in figure 4. The diagnostic case statistics actually give insight into the model strength and the adequacy of the optimal equation in terms of actual factors. To accept any model, its satisfactoriness must first be checked by an appropriate statistical analysis output.



Design-Expert® Software  
Impact Strength

Color points by value of  
Impact Strength :  
116.5  
70



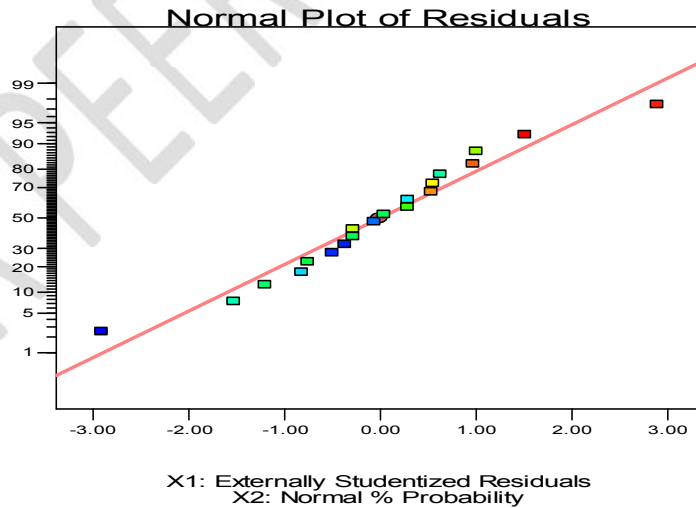
181  
182  
183  
184  
185

**FIG. 5 Statistical Investigation of the Predicted versus Actual Residuals**

Figure 5 shows the statistical plots of the predicted-versus-the the actual data in the response parameter. It reveals the variations in the predicted and the actual data using linear plot, to understand the differences between the predicted and actual response parameter variations.

Design-Expert® Software  
Impact Strength

Color points by value of  
Impact Strength :  
116.5  
70

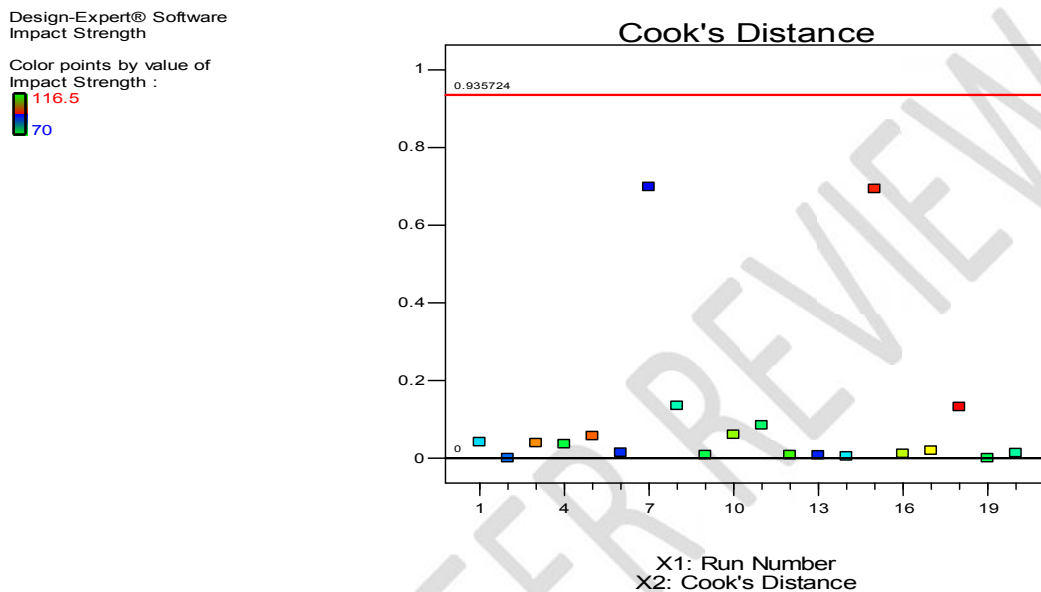


186  
187  
188  
189  
190  
191  
192

**FIG. 6 Normal probability plot of the residuals for optimizing impact strength**

To diagnose the statistical properties of the input factor design, the normal probability plot of residual for impact strength is presented in figure 6. The normal probability plot of studentized residuals was employed to assess the normality of the calculated residuals. The normal probability plot of residuals which is the number of **standard deviations of the actual values** based on the predicted values was employed to ascertain if the residuals (observed – predicted)

193 follows a normal distribution. It is the most significant assumption for checking the sufficiency  
194 of a statistical model. Result of figure 4.43 revealed that the computed residuals are  
195 approximately normally distributed which is an indication that the model developed is  
196 satisfactory.

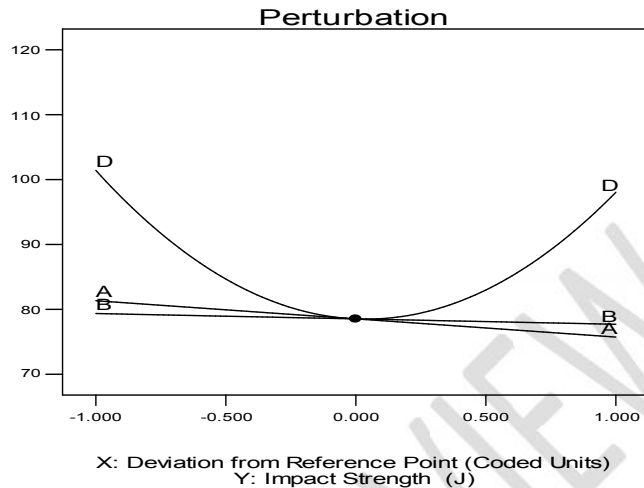


197  
198 **FIG 7 Generated cook distance-versus-impact strength**  
199 To determine the presence of a possible outlier in the experimental data, the cook's distance plot  
200 was generated for the different responses. The cook's distance is a measure of how much the  
201 regression would change if the outlier is omitted from the analysis. A point that has a very high  
202 distance value relative to the other points may be an outlier and should be investigated. The  
203 generated cook's distance is presented in figure 7. The cook's distance plot has an upper bound  
204 of 1.00 and a lower bound of 0.00. Experimental values smaller than the lower bound or greater  
205 than the upper bounds are considered as outliers and must be properly investigated. Result of  
206 figure 4.48 indicates that the data used for this analysis are devoid of any possible outliers thus  
207 revealing the adequacy of the experimental data.

Design-Expert® Software  
 Factor Coding: Actual  
 Impact Strength (J)

Actual Factors  
 A: Gas Flow Rate = 13  
 B: Welding Speed = 117.5  
 C: Welding Voltage = 21  
 D: Welding Current = 210

Factors not in Model  
 C



208  
 209  
 210  
 211  
 212  
 213  
 214  
 215  
 216

**FIG. 8 Perturbation analysis of the impact strength**

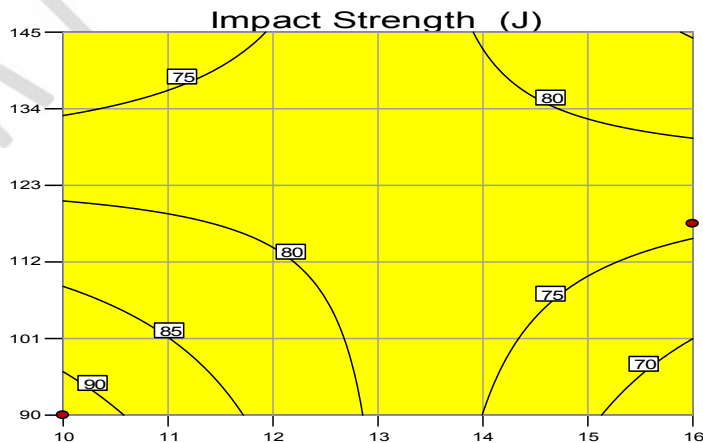
To ascertain the influence of the alterations of process factors to the response variable, perturbation analysis were employed as shown in figure 8. From the results of figure 8, it shows that the disturbances in the response factors by the process factors, and the alterations of the function of the external or internal means of the process factors in the response variables does not make any of the responses to deviate from its reference points. This shows that the deviation of the process factors does not disengage the responses from obtaining a good model and adequate optimization results.

Design-Expert® Software  
 Factor Coding: Actual  
 Impact Strength (J)

● Design Points  
 116.5  
 70

X1 = A: Gas Flow Rate  
 X2 = B: Welding Speed

Actual Factors  
 C: Welding Voltage = 21  
 D: Welding Current = 210



X1: A: Gas Flow Rate  
 X2: B: Welding Speed

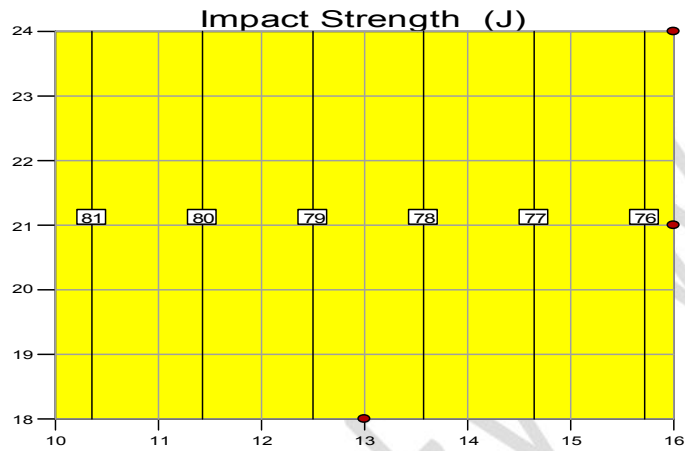
217  
 218  
 219  
 220

**FIG. 9 Contour plot of impact strength Influenced by Gas Flow Rate and Speed**

From the results, the analyses in figure 9 express the influence of the input factors in the responses from the minimum bounded region of the response to the maximum bounded region of

221 the response. It expressed that decrease in gas flow rate and welding speed will increase the  
 222 impact strength.

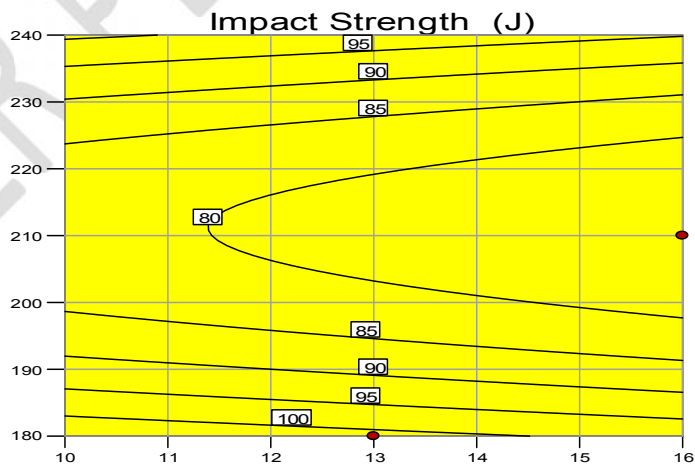
Design-Expert® Software  
 Factor Coding: Actual  
 Impact Strength (J)  
 ● Design Points  
 116.5  
 70  
 X1 = A: Gas Flow Rate  
 X2 = C: Welding Voltage  
 Actual Factors  
 B: Welding Speed = 117.5  
 D: Welding Current = 210



X1: A: Gas Flow Rate  
 X2: C: Welding Voltage

223  
 224 **FIG. 10 Contour plot of the impact strength Influenced by the Gas Flow Rate and Voltage**  
 225 From the results, the analyses in figure 10 express the influence of the input factors in the  
 226 responses from the minimum bounded region of the response to the maximum bounded region of  
 227 the response. It expressed that decrease in gas flow rate increase the impact strength while  
 228 voltage has no influence in the increase or decrease of the impact strength.

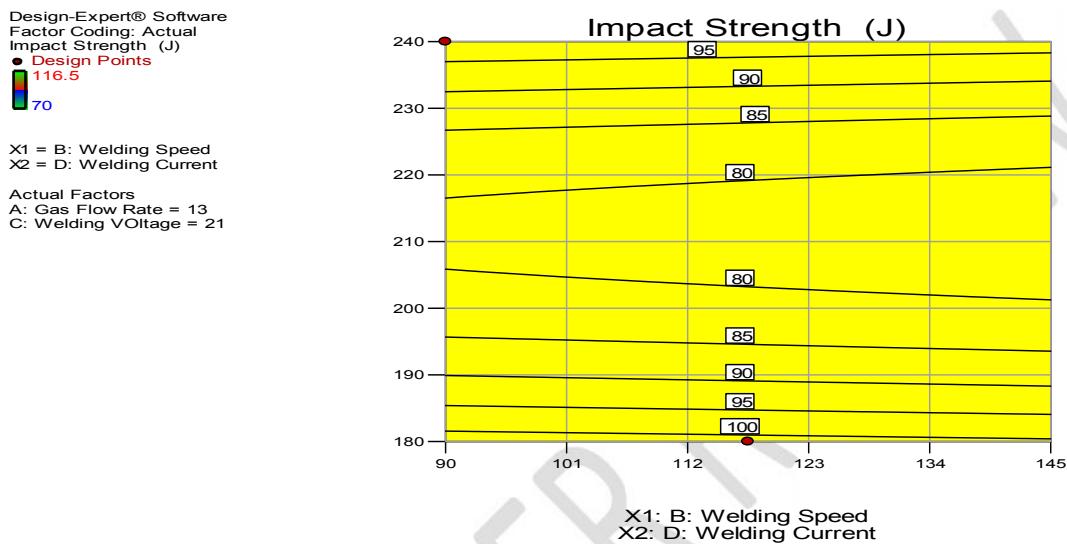
Design-Expert® Software  
 Factor Coding: Actual  
 Impact Strength (J)  
 ● Design Points  
 116.5  
 70  
 X1 = A: Gas Flow Rate  
 X2 = D: Welding Current  
 Actual Factors  
 B: Welding Speed = 117.5  
 C: Welding Voltage = 21



X1: A: Gas Flow Rate  
 X2: D: Welding Current

229  
 230 **FIG. 11 Contour Plot of the Impact Strength Influenced by the Gas Flow Rate and Current**  
 231

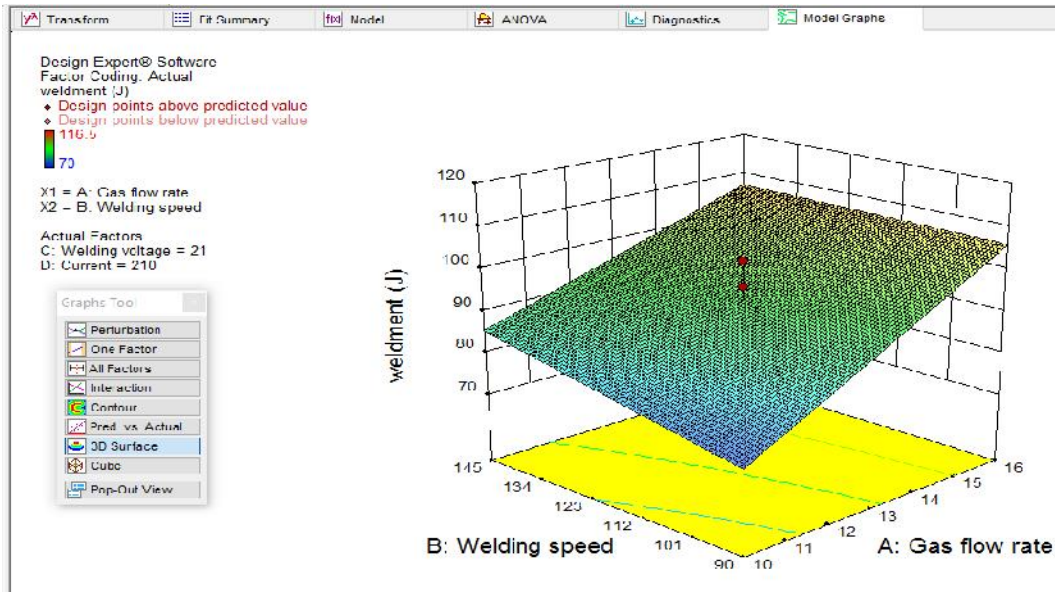
232 From the results, the analyses in figure 11 expressed that increase in gas flow rate increase the  
 233 impact strength while current from its initial decrease the impact strength and at a point starts to  
 234 increase the impact strength. This shows that the selection of the current will be carefully done  
 235 due to its effects to impact strength.



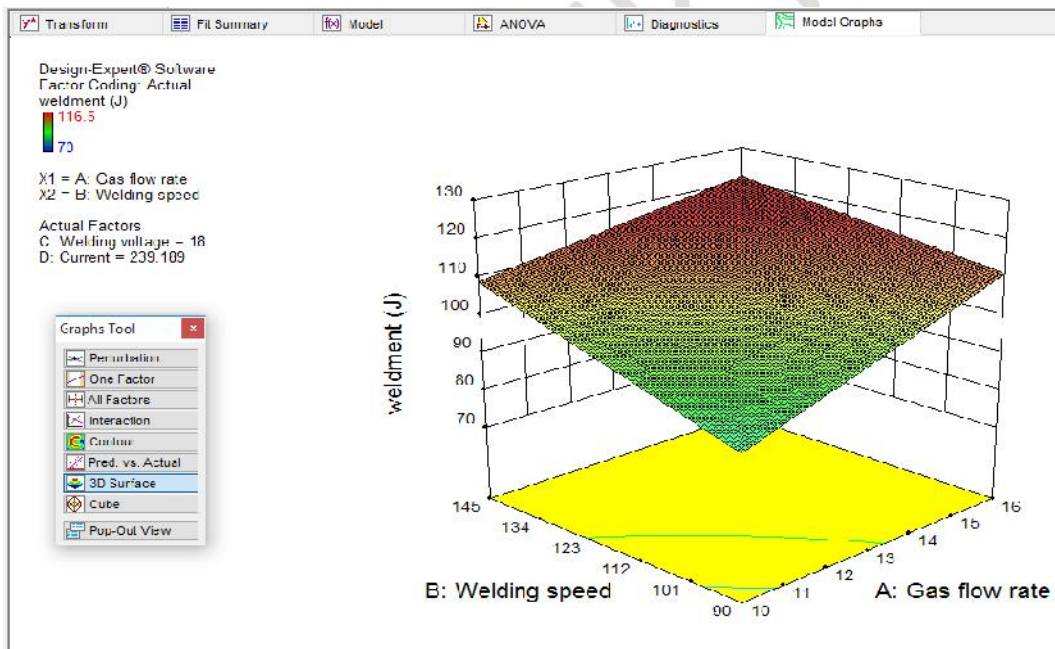
236 **FIG. 12 Contour Plot of the Impact Strength Influenced by the Speed and Current**

237  
 238  
 239 From the results, the analyses in figure 12 expressed that increase in gas flow rate increase the  
 240 impact strength while current from its initial decrease the impact strength and at a point starts to  
 241 increase the impact strength. This shows that the selection of the current will be carefully done  
 242 due to its effects to impact strength. However, the decrease in welding speed will increase the  
 243 impact strength.

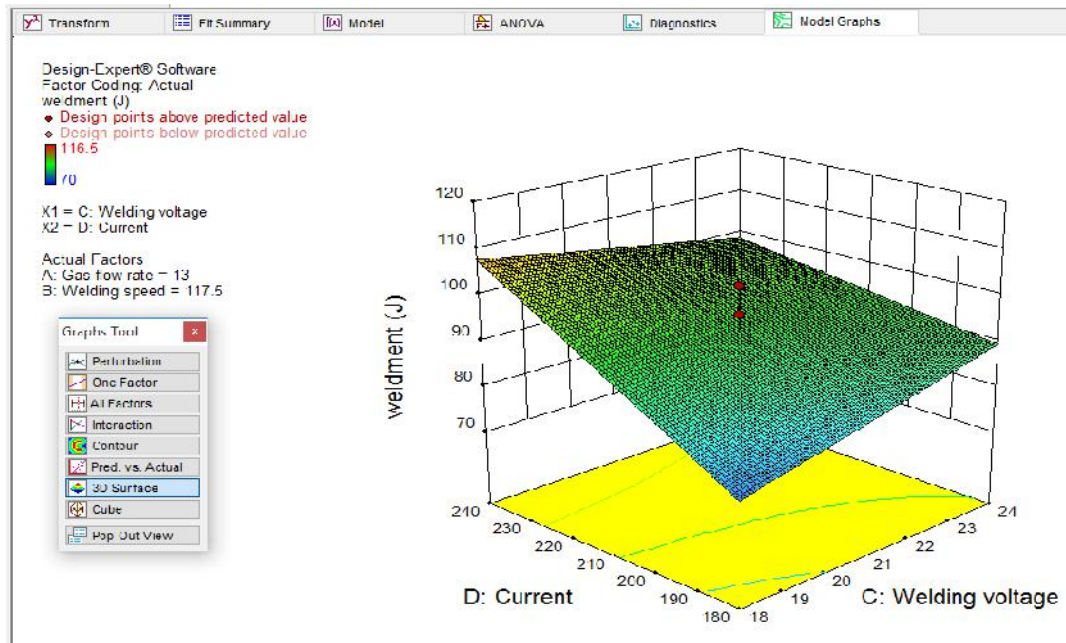




244  
 245 **FIG. 13 Effects of process factors (with CD factors ratio of 50:50) on the impact strength**  
 246 To study the effect of process factors with welding voltage and welding current at its average,  
 247 figure 13 was presented.



248  
 249 **FIG. 14 Effects of process factors (with CD factors ratio of 10:90) on the impact strength**  
 250 To study the effect of process factors with welding voltage and welding current at its ratio of  
 251 10:90, figure 14 was presented.



252  
 253 **FIG. 15 Effect of process factors (with AB factors ratio of 50:50) on the impact strength**  
 254 Figures 13-15 express the 3-dimensional (3D) response surface plots of impact strength on heat  
 255 zone and its significant effects on process factors.

256  
 257 **4. DISCUSSION OF RESULTS**

258 In this study, central composite design was employed owing to its simplicity and flexibility to  
 259 variable adjustment and analysis of process interaction relating to process factors combination.  
 260 The design and analysis was executed with the aid of statistical tool. For this particular problem,  
 261 Design Expert 10.0.1 was employed. However, using response surface method, the results of the  
 262 statistical evaluation for the selected process parameters and response parameter were observed.  
 263 Analysis of the model standard error was employed to assess the suitability of process factor and  
 264 response variables using the central composite design model in response surface to analyze  
 265 statistically, the impact strength on the weldment. The computed ANOVA of design responses  
 266 was presented in figure 2. From the results, the model F-value of 3.31 implies that the model is  
 267 significant. There is only a 4.29% chance that an F-Value this large could occur due to noise.  
 268 Values of "Prob > F" less than 0.0500 indicate model terms are significant. The "Lack of Fit F-  
 269 value" of 0.35 implies the Lack of Fit is not significant relative to the pure error. There is 86.09%

270 chance that a "Lack of Fit F-value" this large could occur due to noise. Non-significant lack of fit  
271 is good for the model fitness.

272 From the result of figure 3, it was observed that the "Predicted R-Squared" value of null is  
273 obtained. In case(s) where leverage of 1.0000 is obtained, Predicted R-Squared and PRESS  
274 statistic are not defined. However, the R-Squared value of the model is 0.8971 while the  
275 Adjusted R-Squared value of the model is 0.7827. "Adequate Precision" measures the signal to  
276 noise ratio. A ratio greater than 4 is desirable. The computed ratio of 8.724 as observed in  
277 figure 3 indicates an adequate signal. This model can be used to navigate the design space.  
278 Variance inflation factor (VIF) less than 10.00 calculated for all the terms in the design indicate a  
279 significant model in which the variables are correlated with the response.

280 Experimental values smaller than the lower bound or greater than the upper bounds are  
281 considered as outliers and must be properly investigated. Result of figure 7 indicates that the data  
282 used for this analysis are devoid of any possible outliers thus revealing the adequacy of the  
283 experimental data.

284 **Figure 13 shows the process factors ratio of 50 to 50 (in current and voltage).** It can be  
285 observed that response (impact strength) increases the welding speed (B) and the gas flow rate  
286 (A). This shows that increase or decrease on the process factors affect the response variable. In  
287 Figure 14, gas flow rate (A) and welding speed (B) were hold at a mix ratio of 50 to 50 or at its  
288 mean which was used to determine the influence of other process factors to the response. It was  
289 observed that increase in current (D), will increase the response(impact strength on weldment).  
290 In addition the geometry of the surface was observed to be concave.

291 In Figure 15, a ratio of 10 to 90 in welding voltage (C) and welding current (D) was used. It  
292 was observed that increase in welding speed (B) and gas flow rate (A) process factors, increases  
293 the response(impact strength on weldment). This shows the lower the welding voltage (C) and  
294 higher the welding current (D) will increase the impact strength on weldment which will  
295 influence and enhance the increase on welding speed and gas flow rate of the process factors to  
296 its response. The 3D surface plot as observed in figures 13-15, show the relationship between the  
297 process factors (current, gas flow rate, speed and voltage), against the response variable (impact  
298 strength). It is a 3-dimensional surface plot which was employed to give a clearer concept of the

299 surface. Although not as useful as the contour plot for establishing coordinates, this view  
300 provides a clearer picture of the surface. It was observed from Figures 13-15 that the input  
301 factors has significant influence on the surface geometry and the overall contributions towards  
302 the response variable (impact strength).

## 303 **5 CONCLUSIONS**

304 A close examination of the **mild steel-clad** welding metal was experimented with the input  
305 parameters of current, voltage, speed and gas flow rate to predict and to analyze the mild steel  
306 cladding weld metal response parameter (impact strength) using response surface method.  
307 Welding parameters were carefully selected. The results of the statistical investigation revealed  
308 the model F-value of 3.31 is significant. There is only a 4.29% chance that an F-Value this large  
309 could occur due to noise. Values of "Prob > F" less than 0.0500 indicate model terms are  
310 significant. The "Lack of Fit F-value" of 0.35 implies the Lack of Fit is not significant relative to  
311 the pure error. There is 86.09% chance that a "Lack of Fit F-value" this large could occur due to  
312 noise. Non-significant lack of fit is good for the model fitness. It was observed that the R-  
313 Squared value of the model is 0.8971 while the Adjusted R-Squared value of the model is  
314 0.7827. Adequate Precision measures the signal to noise ratio and a ratio greater than 4 is  
315 desirable. The computed ratio of 8.724 as observed which indicates an adequate signal. This  
316 model can be used to navigate the design space. Variance inflation factor (VIF) less than 10.00  
317 calculated for all the terms in the design indicate a significant model in which the variables are  
318 correlated with the response. In response surface plots and contour plots, the process parameters  
319 influence the impact strength except voltage, which has no effect on the response parameter.

320 The performed experiment will appraise the knowledge of mild steel cladding weld  
321 formulation and composition in tungsten inert gas (TIG) welding system and also in  
322 industrialization. The experimental analysis and its statistical evaluation will help in decision  
323 making systematically mostly in industrialization were the product is more utilized.

324

## 325 **REFERENCES**

326 Achebo Joseph Ifeanyi (2016). Development of Compositions of **Aluminum** Welding Fluxes  
327 Using Statistical Method. *Proceedings of the International MultiConference of Engineers*

328 *and Computer Scientists*. 2009 Vol II IMECS 2009, March 18 - 20, 2009, Hong Kong.  
329 All content following this page was uploaded by Joseph Achebo on 13 August 2016.

330 Eutimio Gustavo Fernandez Nunez, Rodolfo Valdes Veliz, Bruno Labate Vale da Costa,  
331 Alexandre Goncalves de Rezende and Aldo Tonso, (2013). Using Statistical Tools for  
332 Improving Bioprocesses. *Asian Journal of Biotechnology*, 5: 1-20. DOI:  
333 10.3923/ajbkr.2013.1.20; URL: <https://scialert.net/abstract/?doi=ajbkr.2013.1.20>

334 Liem Ferryanto (2018). Designing and Analyzing Experiments with Mixtures. Retrieved online  
335 on May, 12<sup>th</sup>, 2018.

336 Marko, Angelina; Graf, Benjamin; Rethmeier, Michael (2017): Statistical analysis of weld bead  
337 geometry in Ti6Al4V laser cladding. Comparison of central composite design and five  
338 step full factorial test plan. *MATERIALS SCIENCE (S36); MP Materials Testing*; ISSN  
339 0025-5300; v. 59(10); p. 837-843

340 Mastanaiah P.; Abhay Sharma; Madhusudhan Reddy G. (2014): Process parameters-weld bead  
341 geometry interactions and their influence on mechanical properties: A case of dissimilar  
342 aluminium alloy electron beam welds. *Defence Technology*; Volume 14, Issue 2, April  
343 2018, Pages 137-150, sciencedirect, <https://doi.org/10.1016/j.dt.2018.01.003>.

344 Nuri Akkas, Durmuş Karayel, Sinan Serdar Ozkan, Ahmet Oğur, and Bayram Topal (2013):  
345 Modeling and Analysis of the Weld Bead Geometry in Submerged Arc Welding by  
346 Using Adaptive Neurofuzzy Inference System. *Mathematical Problems in Engineering*;  
347 Volume 2013, Article ID 473495, 10 pages, <http://dx.doi.org/10.1155/2013/473495>.

348 Palani P. K. and Murugan N. (2006): Development of mathematical models for prediction of  
349 weld bead geometry in cladding by flux cored arc welding, *The International Journal of*  
350 *Advanced Manufacturing Technology*, October 2006, Volume 30, Issue 7–8, pp 669–  
351 676; DOI 10.1007/s00170-005-0101-2

352 Stefano Farris, Carlo Alessio Cozzolino, Laura Introzzi, Luciano Piergiovanni (2009). Effects of  
353 different sealing conditions on the seal strength of polypropylene films coated with a bio-



354 based thin layer. *Packaging Technology and Science*. DOI: 10.1002/pts.861, Volume 22,  
355 Issue 6, October 2009, Pages 359–369. Copyright 2009, John Wiley & Sons, Ltd  
356 Xu W. H., Lin S. B., Fan C. L., Zhuo X. Q., and Yang C. L. (2014): Statistical modelling of weld  
357 bead geometry in oscillating arc narrow gap all-position GMA welding. *The International*  
358 *Journal of Advanced Manufacturing Technology*; June 2014, Volume 72, Issue 9–12, pp  
359 1705–1716; DOI 10.1007/s00170-014-5799-2  
360

UNDER PEER REVIEW