#### STATISTICAL EVALUATION OF THE IMPACT STRENGTH ON MILD STEEL CLADDING WELD METAL GEOMETRY

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1 2

#### 5 Abstract

6 The research focused on statistical evaluation of the impact strength on mild steel cladding weld metal geometry. The weld specimen of length 60 UNITS?? by width 40 and thickness of 10 was 7 used for the experiment. A butt joint method was prepared and tungsten inert gas welding 8 9 process was used to perform the twenty (20) experimental runs. A response surface method was applied to model and to analyze statistically the welded metal bead geometry. The statistical 10 result expressed that the model developed is significance. However, there is only 4.29% chance 11 that an F-Value could occur due to noise. Probability values that is less than 0.0500 indicate that 12 the model terms are significant. In this research, there is 86.09% chance that a Lack of Fit of F-13 value which is this large could occur due to noise. Non-significant lack of fit is good for the 14 15 model fitness. It was observed that the R-Squared value of the model is 0.8971 while the Adjusted R-Squared value of the model is 0.7827. Adequate Precision measures the signal to 16 noise ratio and a ratio greater than 4 is desirable. However, the computed ratio of 8.724 was 17 observed which indicates an adequate signal. The results of response surface plots and contour 18 plots observe that the process parameters influence the impact strength of the weld bead 19 geometry except voltage, which has no effect on the output parameter. The statistical 20 21 investigation reveals the statistical solutions necessary to portray the parameters under study.

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Keywords: Mild steel, impact strength, response surface, ANOVA, bead geometry, welding and
 Statistics

#### 25 **1. INTRODUCTION**

In today's Industrial world and its economy, metals and steels have been employed for domestic, 26 agricultural, construction and several other purposes due to its variations in ductility, corrosion 27 and rust resistance, and its other properties that makes the material a unique and irresistible 28 29 materials in Industrialization. Industrialization world utilize these materials mainly because of their mechanical properties as well as their excellent corrosion resistance. Cladding weld has 30 been the methods of joining these metals because of the low price and high quality of the 31 welding process (Palani and Murugan, 2006b). On the other hand, it is also imperative to 32 highlight that during welding overlaying many discontinuities are produced, which acts as stress 33 raisers that can lead to a decrease in the life of the weld. Depending on weld parameters used, 34 deposition rates, dilution rates and mild steel metal in use. The shape of weld bead would 35 influence the weld metal cooling which would alter the weld, metal transformation. Welding 36 parameters are to be carefully selected (Kannan and Murugan, 2006). This loss and pick-up in 37 welding will influence the mechanical properties of the weld metal. Although weld metal 38

39 properties are primarily controlled by the consumable composition of the shielding gas which 40 can directly influence the strength and ductility of a weld. Its paramount to understand the 41 statistical influence of process parameters in mild steel cladding weld bead geometry (Murugan 42 and Gunaraj, 2005).

This study investigates the application of statistics to investigate and to analyze the influence of cladding weld metal geometry in mild steel using response surface method with the application of TIG welding method. Therefore, the main objective of the study is to determine and to evaluate the statistical solutions and its influences of the impact strength in mild steel cladding weld metal bead geometry.

#### 48 2. PROCESSES OF WELDING

These processes use a welding power supply to create and maintain an electric arc between an electrode and the base material to melt metals at the welding point. They can use either direct current or alternating current and consumable or non-consumable electrodes. The welding region is sometimes protected by some type of inert or semi-inert gas, known as a shielding gas, and filler material is sometimes used as well (Lincoln, 2014).

## 54 2.1 Review of Related Literature under Study

Palani and Murugan (2006a) expressed the mechanical and corrosion-resistant properties of the 55 coated components depend on the geometries of the coated beads, which in turn are controlled by 56 the process parameters. Therefore, it is essential to study the effect of the process parameters on 57 the cord geometry to allow effective control of these parameters. The above objective can be 58 easily achieved by developing equations to predict the dimensions of the weld bead in terms of 59 process parameters. The models developed were reviewed for their suitability. Confirmation 60 experiments were also performed and the results show that the developed models can predict the 61 62 geometries and the dilution of the beads with reasonable precision. It was observed from the research that the interactive effect of the parameters of the process in the geometry of the account 63 is significant and cannot be neglected. Eutimio et al (2013), shows that most of statistical tools 64 currently applied in the bioprocess area were classified. The main three categories were: fair 65 66 comparison of results, mathematical modeling for little studied systems and taking advantage of large volume of data for enhance robustness and efficiency. However, a chart was constructed 67

for guiding researchers to select the correct statistical technique according to the specificbioprocess problem.

70 Achebo (2016) describes the process of developing a model that relates the shear stresses in a gas welded aluminum alloy weldment with the corresponding flux constituent elements that 71 make up the flux composition. The weldments made from the 13 flux compositions were 72 subjected to evaluation by some professional welders whose judgments about the quality of the 73 74 weldments were evaluated by using the rank correlation coefficient method. Stefano et al (2009) present the results of a research through the design of an experimental technique on the influence 75 of temperature, the residence time and the pressure of the bar in the resistance to heat sealing of 76 oriented polypropylene films coated with a thin layer of gelatin. This chemo-metric approach 77 allowed to achieve a complete understanding of the effect of each independent factor in the two 78 different responses considered as a measure of the force required to break the link through the 79 sealed interface. 80

Marko et al (2017), express that the process of laser cladding has become more important 81 during recent years because of its broad application for cladding, repair or additive 82 manufacturing. For high quality and reliability of the repaired components, it is necessary to 83 adjust the weld bead geometry to the specific repair task. The bead geometry influences the 84 metallurgical bonding and the degree of dilution as well as the formation of defects like pores or 85 cracks. The results show, the essential effects are detected with a full factorial test plan as well as 86 87 with a central composite design. Merely the effect strength could not always be specified unambiguously. Mastanaiah et al (2014) described the Prediction of weld bead geometry is 88 always an interesting and challenging research as it involves understanding of complex multi 89 input and multi output system. The weld bead geometry has a profound impact on the load 90 91 bearing capability of a weld joint. The results of investigation suggests the effective thickness of weld, a geometric parameter of weld bead has the most significant influence on tensile breaking 92 load of dissimilar weld joint. The observations on bead geometry and the mechanical are 93 correlated with detailed metallurgical analysis. Xu et al (2014) described the oscillating arc 94 95 narrow gap all-position gas metal arc welding process was developed to improve efficiency and quality in the welding of thick-walled pipes. The developed models were checked for their 96

97 adequacy and significance by ANOVA, and the effects of wire feed rate, travel speed, dwell time, oscillating amplitude and welding position on weld bead dimension were studied. Finally, 98 the optimal welding parameters at welding positions of  $0^{\circ}$  to  $180^{\circ}$  were obtained by numerical 99 optimization using RSM. Nuri et al (2013) study is aimed at obtaining a relationship between the 100 101 values defining bead geometry and the welding parameters and also to select optimum welding parameters. The welding process parameters that have the most effect on bead geometry are 102 103 considered and the other parameters are held as constant. Then, the relationship between the welding parameters is modeled by using artificial neural network and neurofuzzy system 104 approach. The models developed are compared with regard to accuracy and the appropriate 105 welding parameters values can be easily selected when the models improve. 106

## **3. DESIGN OF EXPERIMENT**

Design of experiment is a scientific approach of combining input parameters optimally so as to optimize a target response and this can be achieved by using computer software like design expert. For proper polynomial approximation, experimental designs are used to collect the data. In this research, central composite design in response surface method was used to generate the experimental runs. Furthermore, response surface method was used to evaluate, model and analyze the data statistically which generates the statistical results.

# 114 **3.1 Identifying the Range of Input Parameters**

115 The key parameters considered in this work are welding current, gas flow rate, welding speed 116 and voltage. The range of process parameters obtain from literature is shown in the table below.

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 TABLE 1
 Process parameters at Low and High Levels

		· · · · · · · · · · · · · · · · · · ·			
Parameter	Units	Symbol	Low	High	
Current	Amp	A	180	240	
Gas flow rate	Lit/min	F	10	16	
Voltage	Volt	V	18	24	
Welding speed	Mm/s	S	90	145	

Impact testing machine is a machine used for the impact testing analysis. It is used to test the impact strength of the materials to determine the energy or strength of the materials at a specific location of the material basically at the weldment and other specified locations the researcher wished to determine the strength in that location. It measures the unit of the material strength in Joules.



# 124 Fig. 1: Impact Testing Setup

125 In the fabrication industry materials standard and specification plays a very vital role in 126 achieving good weld quality. The welding parameter specification is shown in the table below.

# 127 **3.5** Method of Data Collection

The central composite design matrix was developed using the design expert software, producing 20 experimental runs. The input parameters and output parameters make up the experimental matrix and the responses recorded from the weld samples was used as the data. The input process factors are welding current, welding voltage, welding speed and gas flow rate. The output process response is impact strength of the weldment. The input and output parameters were analyzed statistically modeled and optimized.

# 1343.6Method of Data Analysis

Response Surface Methodology (RSM) Engineers often search for the conditions that would investigate the process of interest. RSM is one of the techniques currently in widespread usage to describe the performance of the welding process and find the statistical investigation of the responses of interest. RSM is a set of mathematical and statistical techniques that are useful for modeling and predicting the response of interest affected by several input variables with the aim of optimizing this response.

# 141 4.1 Modeling and Statistical evaluation using Response Surface Technique

In this paper, the researcher revealed a mathematical relationship between selected process factors, namely; current, speed, gas flow rate and voltage to the response variable. The response variable of interest is impact strength of the material.

Transform	Elt Sur	mary	[(A) Model		ANOVA	Diagnos
Analysis of var	lance table [Par	tlal sum of	squares - T	vpe III1		^
	Sum of		Mean	F	p-value	
Source	Squares	П	Square	Value	Prob > F	
Model	2718.36	10	271.84	3.31	0.0429	significant
A-Gas flow re	04.50	1	04.50	1.03	0.3370	
D-Welding st	351.13	1	351.13	4.27	0.0000	
C-Welding ve	7.54	1	7.54	0.092	0.7688	
D-Current	40.50	1	40.50	0.49	0.5003	
AB	25.30	1	25.30	0.31	0.5924	
AC	1809.01	1	1809.01	22.02	0.0011	
NU	1.70	1	1.70	0.021	0.8888	
BC:	0.36	1	0.36	4.398E-003	0.9486	
BD	49.82	1	49.82	0.61	0.4561	
CD	14.85	7	14.85	0.18	0.6807	
Residual	739.30	9	82 14			
Lack of Fit	224.38	.5	44 88	0.35	0 8609 //	ol significant
Pure Error	514.91	4	128.73			
Cur Tulal	3457.66	19				

## 146 Fig. 2: Model Significance of the Impact Strength using ANOVA

Analysis of the model standard error was employed to assess the suitability of process factor and 147 response variables using the central composite design model in response surface to optimize the 148 impact strength on the weldment. The computed ANOVA of design responses was presented in 149 figure 2. From the results of figure 2, the Model has ten (10) degree of freedom, with the model 150 F-value of 3.31 which implies that the model is significant. There is only a 4.29% chance that an 151 F-Value this large could occur due to noise. Values of "Prob > F" less than 0.0500 indicate 152 model terms are significant. In this case A, D, AC are significant model terms. Values greater 153 than 0.1000 indicate the model terms are not significant. The "Lack of Fit F-value" of 0.35 154 implies the Lack of Fit is not significant relative to the pure error. There is 86.09% chance that a 155 "Lack of Fit F-value" this large could occur due to noise. Non-significant lack of fit is good for 156 the model fitness. 157

Std. Dev.	6.91	R-Squared	0.8971	
Mean	91.78	Adj R-Squared	0.7827	
C.V. %	7.52	Pred R-Square	N/A	
PRESS	N/A	Adeq Precisior	8.724	
2 Log Likeliho	118.08	BIC	151.03	
		AICc	173.08	
Case(s) with leve	erage of 1.0000: Pre	ed R-Squared and PRESS	statistic not defined	
'Adea Precision" r	measures the signa	I to noise ratio. A ratio ore	ater than 4 is desirable.	Your



160 To validate the adequacy of the model based on its ability to maximize the impact strength. the goodness of fit statistics was presented in figure 3. From the result of figure 3, it was 161 162 observed that the "Predicted R-Squared" value of nill is obtained. In case(s) where leverage of 1.0000 is obtained, Predicted R-Squared and PRESS statistic are not defined. However, the R-163 164 Squared value of the model is 0.8971 while the Adjusted R-Squared value of the model is 0.7827. "Adequate Precision" measures the signal to noise ratio. A ratio greater than 4 is 165 166 desirable. The computaed ratio of 8.724 as observed in figure 3 indicates an adequate signal. This model can be used to navigate the design space. Variance inflation factor (VIF) less than 167 10.00 calculated for all the terms in the design indicate a significant model in which the variables 168 169 are correlated with the response.

Transform	Fit	Summary	f(x) Model				Diagnostics	Mo	del Graphs
Response 5	3	weldment			Transform:	None			
Diagnoe	tice Caee S	tatistics			Internally	Externally		Influence on	
Run	Actual	Predicted			Studentized	Studentized	Cook's	Fitted Value	Standar
Order	Value	Value	Residual	Leverage	Residual	Residual	Distance	DFFITS	Order
1	80.00	75.42	4.58	0.553	0.991	0.990	0.110	1.101	15
2	75.00	74.54	0.46	0.076	0.190	0.179	0.023	0.477	0
3	110.00	109.54	0.46	0.876	0.190	0.179	0.023	0.477	4
4	90.50	88.68	1.82	0.876	0.748	0.729	0.359	1.935	7
5	112.00	111.54	0.46	0.876	0.190	0.179	0.023	0.477	5
6	72.00	70.18	1.82	0.876	0.748	0.729	0.359	1.935	6
Ĺ	/0.00	/0.00	0.000	1.0001					9
8	85.00	90.81	5.81	0.260	0.977	0.974	0.030	0.577	13
9	90.00	92.92	-2.92	0.053	-0.435	-0.414	0.001	-0.098	18
10	100.00	98.67	1.33	0.553	0.288	0.273	0.009	0.303	12
11	88.50	87.17	1.33	0.553	0.288	0.273	0.009	0.303	11
12	96.00	92.92	3.08	0.053	0.458	0.437	0.001	0.103	19
10	71.50	71.04	0.46	0.876	0.190	0.179	0.023	0.477	2
14	81.00	92.92	-11.92	0.053	-1.774	-2.073	0.016	-0.489	21
15	115.00	110.42	4.58	0.553	0.991	0.990	0.110	1.101	16
16	102.00	92.92	9.08	0.053	1.351	1.426	0.009	0.336	17
17	105.0 <mark>0</mark>	103.18	1.82	0.876	0.748	0.729	0.359	1.935	1
18	116.50	114.68	1.82	0.876	0.748	0.729	0.359	1.935	3
19	89.50	92.92	-3.42	0.053	-0.509	-0.487	0.001	-0.115	20
20	86.00	95.04	-9.04	0.260	-1.521	-1.664	0.074	-0.985	14

170 171

Fig. 4: Diagnostics Statistics Report of Impact Strength (J)

The diagnostics case statistics report which shows the observed values of each response variable (impact strength) against their predicted values is presented in figure 4. The diagnostic case statistics actually give insight into the model strength and the adequacy of the optimal equation in terms of actual factors. To accept any model, its satisfactoriness must first be checked by an appropriate statistical analysis output.



Design-Expert® Sof Impact Strength

points by the strength

**1**10

X1: Actual X2: Predicted

- Statistical Investigation of the Predticted versus Actual Residuals 178 Fig. 5
- Figure 5 shows the statistical plot of the predicted versus the the actual data in the response 179
- parameter. It reveals the variations in the predicted and the actual data using linear fitted line, to 180
- understand the differences between the predicted and actual response parameter variations. 181



#### 182 Fig. 6 Normal Probability Plot of Residuals for Impact Strength 183

To diagnose the statistical properties of the input factor design, the normal probability plot of 184 residual for impact strength is presented in figure 6. The normal probability plot of studentized 185 residuals was employed to assess the normality of the calculated residuals. The normal 186 probability plot of residuals which is the number of standard deviations of actual values based on 187 the predicted values was employed to ascertain if the residuals (observed – predicted) follows a 188 normal distribution. It is the most significant assumption for checking the sufficiency of a 189 statistical model. Result of figure 6 revealed that the computed residuals are approximately 190 191 normally distributed which is an indication that the model developed is satisfactory.



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To determine the presence of a possible outlier in the experimental data, the cook's distance plot 194 was generated for the different responses. The cook's distance is a measure of how much the 195 regression would change if the outlier is omitted from the analysis. A point that has a very high 196 distance value relative to the other points may be an outlier and should be investigated. The 197 generated cook's distance is presented in figure 7. The cook's distance plot has an upper bound 198 of 1 and a lower bound of 0. Experimental values smaller than the lower bound or greater than 199 the upper bounds are considered as outliers and must be properly investigated. Result of figure 7 200 indicates that the data used for this analysis are devoid of any possible outliers thus revealing the 201 adequacy of the experimental data. 202



204 Fig. 8: Perturbation Analysis of the Impact Strength

To ascertain the influence of the alterations of process factors to the response variable, perturbation analysis were employed as shown in figure 8. From the results of figure 8, it shows that the disturbances in the response factors by the process factors, and the alterations of the function of the external or internal means of the process factors in the response variables does not make any of the responses to deviate from its reference points. This shows that the deviation

- 210 of the process factors does not disengage the responses from obtaining a good model and
- 211 adequate optimization results.



- Fig. 9 Contour Plot of Impact Strength Influenced by Gas Flow Rate and Speed
- From the results, the analyses in figure 9 express the influence of the input factors in the
- responses from the minimum bounded region of the response to the maximum bounded region of
- the response. It expressed that decrease in gas flow rate and welding speed will increase the
- 217 impact strength.



- Fig. 10 Contour Plot of Impact Strength Influenced by Gas Flow Rate and Voltage
- From the results, the analyses in figure 10 express the influence of the input factors in the responses from the minimum bounded region of the response to the maximum bounded region of
- the response. It expressed that decrease in gas flow rate increase the impact strength while
- voltage has no influence in the increase or decrease of the impact strength.



- 224
- Fig. 11 Contour Plot of Impact Strength Influenced by Gas Flow Rate and Current
- From the results, figure 11 indicates that an increase in gas flow rate increases the impact

strength while current from its initial decrease the impact strength and at a point starts to increase

- the impact strength. This shows that the selection of the current will be carefully done due to its
- effects to impact strength.

Design-Expert® Software		Impact Strength	(J)
Impact Strength (J)	240 -	95	
<ul> <li>Design Points</li> <li>116.5</li> </ul>		90	
70			
	230	85	
X1 = B: Welding Speed			
X2 = D: Welding Current	220 -	80	
Actual Factors A: Gas Flow Rate = 13			
C: Welding VOltage = 21	210 -		
	210		
		80	
	200 -		
		85	
	190		
		95	
	180	100	
	90	101 112 123	134 145
		X1: B: Welding Spee	d
		X2: D: Welding Curre	nt

230
 231 Fig. 12 Impact Strength Contour Plot Influenced by Speed and Current

From the results, the analyses in figure 12 expressed that increase in gas flow rate increase the impact strength while current from its initial decrease the impact strength and at a point starts to increase the impact strength. This shows that the selection of the current will be carefully done due to its effects to impact strength. However, the decrease in welding speed will increase the impact strength.



- 238 Fig. 13 Effects of Process Factors (with CD factors ratio of 50:50) on the Impact Strength
- 239 To study the effect of process factors with welding voltage and welding current at its average,
- figure 13 was presented.



# 241

- Fig. 14 Effects of Process Factors (with CD factors ratio of 10:90) on the Impact Strength
- To study the effect of process factors with welding voltage and welding current at its ratio of
- 10:90, figure 14 was presented.



Fig. 15 Effects of Process Factors (with AB Factors Ratio of 50:50) on the Impact Strength
 Fig. 15 Effects of Process Factors (with AB Factors Ratio of 50:50) on the Impact Strength

Figures 13-15 express the 3-dimensioal (3D) response surface plots of impact strength on heat zone and its significant effects on process factors.

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## 251 4. Discussion of Results

In this study, central composite design was employed owing to its simplicity and flexibility to 252 variable adjustment and analysis of process interaction relating to process factors combination. 253 The design and analysis was executed with the aid of statistical tool. For this particular problem, 254 Design Expert 10.0.1 was employed. However, using response surface method, the results of the 255 statistical evaluation for the selected process parameters and response parameter were observed. 256 Analysis of the model standard error was employed to assess the suitability of process factor and 257 response variables using the central composite design model in response surface to analyze 258 statistically, the impact strength on the weldment. The computed ANOVA of design responses 259 was presented in figure 2. From the results, the model F-value of 3.31 implies that the model is 260 significant. There is only a 4.29% chance that an F-Value this large could occur due to noise. 261 Values of "Prob > F" less than 0.0500 indicate model terms are significant. The "Lack of Fit F-262 value" of 0.35 implies the Lack of Fit is not significant relative to the pure error. There is 86.09% 263

chance that a "Lack of Fit F-value" this large could occur due to noise. Non-significant lack of fitis good for the model fitness.

266 From the result of figure 3, it was observed that the "Predicted R-Squared" value of nill is obtained. In case(s) where leverage of 1.0000 is obtained, Predicted R-Squared and PRESS 267 268 statistic are not defined. However, the R-Squared value of the model is 0.8971 while the Adjusted R-Squared value of the model is 0.7827. "Adequate Precision" measures the signal to 269 270 noise ratio. A ratio greater than 4 is desirable. The computated ratio of 8.724 as observed in figure 3 indicates an adequate signal. This model can be used to navigate the design space. 271 272 Variance inflation factor (VIF) less than 10.00 calculated for all the terms in the design indicate a significant model in which the variables are correlated with the response. 273

Experimental values smaller than the lower bound or greater than the upper bounds are considered as outliers and must be properly investigated. Result of figure 7 indicates that the data used for this analysis are devoid of any possible outliers thus revealing the adequacy of the experimental data.

Figure 13 shows the process factors ratio of 50 to 50 (in current and voltage). It was observed that increase in response (impact strength) increases welding speed (B) and gas flow rate (A). This shows that increase or decrease on the process factors affect the response variable. In Figure 14, gas flow rate (A) and welding speed (B) were hold at a mix ratio of 50 to 50 or at its mean which was used to determine the influence of other process factors to the response. It was observed that increase in current (D), will increase the response(impact strength on weldment). In addition the geometry of the surface was observed to be concave.

285 In Figure 15 a ratio of 10 to 90 in welding voltage (C) and welding current (D) was used. It was observed that increase in welding speed (B) and gas flow rate (A) process factors, increases 286 the response(impact strength on weldment). This shows the lower the welding voltage (C) and 287 higher the welding current (D) will increase the impact strength on weldment which will 288 289 influence and enhance the increase on welding speed and gas flow rate of the process factors to its response. The 3D surface plot as observed in figures 13-15, show the relationship between the 290 291 process factors (current, gas flow rate, speed and voltage), against the response variable (impact strength). It is a 3-dimensional surface plot which was employed to give a clearer concept of the 292 293 surface. Although not as useful as the contour plot for establishing coordinates, this view provides a clearer picture of the surface. It was observed from Figures 13-15 that the input 294

factors has significant influence on the surface geometry and the overall contributions towardsthe response variable (impact strength).

## 297 **5. CONCLUSIONS**

A close examination of the mild steel cladding weld metal was experimented with the input parameters of current, voltage, speed and gas flow rate to predict and to analyze the mild steel cladding weld metal response parameter (impact strength) using response surface method. Welding parameters were carefully selected.

The results of the statistical investigation revealed the model F-value of 3.31 is significant. 302 There is only a 4.29% chance that an F-Value this large could occur due to noise. Values of 303 "Prob > F" less than 0.05 indicate model terms are significant. The "Lack of Fit F-value" of 0.35 304 implies the Lack of Fit is not significant relative to the pure error. There is 86.09% chance that a 305 "Lack of Fit F-value" this large could occur due to noise. Non-significant lack of fit is good for 306 the model fitness. It was observed that the R-Squared value of the model is 0.8971 while the 307 Adjusted R-Squared value of the model is 0.7827. Adequate precision measures the signal to 308 noise ratio and a ratio greater than 4 is desirable. The computaed ratio of 8.724 as observed 309 which indicates an adequate signal. This model can be used to navigate the design space. 310 Variance inflation factor (VIF) less than 10 calculated for all the terms in the design indicate a 311 significant model in which the variables are correlated with the response. In response surface 312 plots and contour plots, the process parameters influence the impact strength except voltage, 313 314 which has no effect on the response parameter.

The performed experiment will appraise the knowledge of mild steel cladding weld formulation and composition in tungsten inert gas (TIG) welding system and also in industrialization. The experimental analysis and its statistical evaluation will help in decision making systematically in the industrialization where the product is more utilized.

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