

3
4 **Influence of mixing time on fresh and hardened**
5 **cast-in-place concrete**

6
7
8 **ABSTRACT**

9 An adequate mixing time in concrete casting allows to achieve a homogeneous mass and improve compressive strength and durability. However, the lack of standards for cast-in-place concrete causes that the builders use different mixing times according to the locality usages and customs, which results in a high variability of the expected quality. In this paper, fresh and hardened cast-in-place concrete was evaluated. Seven samples were tested with different mixing time using portable rotary drum mixer. The used materials were ordinary portland cement, water and high absorption aggregates, fine and coarse, coming from a limestone crushing process. The results of the research showed that the mixing time and environmental temperature had no apparent influence on the slump of the mixtures, and trapped air and compressive strength increased slightly with increasing mixing time. Finally, it was found that the recommended mixing time, with rotation speed of 28 RPM, is 2.5 minutes, which differs from the common practice in the study area.

10
11 *Keywords: Mixing time, cast-in-place concrete, rotation speed, compressive strength, slump.*

12
13 **1. INTRODUCTION**

14
15 Concrete is a composite material that contains cement, water, aggregates and often,
16 additives or additions. When these materials have been mixed and hydrated, they generate
17 a chemical reaction forming a homogenous mass, a quality that improve compressive
18 strength and durability. In addition to the water/cement ratio, and the quality of the materials,
19 an important factor that influences the behavior of hardened concrete is the mixing time. The
20 optimum mixing time depends in turn on the type and conditions of the mixer, rotation speed,
21 load size, nature of the materials, and the environmental temperature, therefore, the most
22 efficient mixing time should be determined in the field considering these variables [1]. In
23 Mexico, the recommended mixing time by the NMX C-159-ONNCCE-1999 standard [2] is
24 five minutes after all the materials were loaded, however, in the works, it is almost always
25 about mixing the concrete as quickly as possible, which is due to economic issues, so
26 determining the necessary minimum time is very important. Some minimum mixing times
27 have been specified in several standards and regulations according to the capacity of the
28 mixer, but generally refer to ready-mix concrete. The recommended minimum mixing times
29 for low capacity mixers, are indicated in Table 1.

30
31 **Table 1. Minimum mixing times for low capacity mixers**

32

Loading capacity (m ³)	Minimum time (min)	Reference
0.76	1.0	[3, 4]
<1.5	1.5	[5]
--	1.5	[6]

33

34 According to Neville and Brooks [7], a mixing time of less than one minute causes problems
35 of uniformity and low strength in the concrete. Conversely, a greater time than two minutes
36 does not necessarily means that there is an improvement in those properties. Other authors
37 such as Charonnat and Beitzel [8] in countries of the European Union, as well as Trejo and
38 Chen [9] in the United States, have focused on the study of time and efficiency of the mixing
39 process in prolonged periods because the use of ready-mixed concrete has a high demand.
40 However, in many countries with less technological development, cast-in-place concrete for
41 medium and small works is a frequent practice, carried out in various ways due to the lack of
42 precise specifications to achieve adequate characteristics of workability and compressive
43 strength. This has led to the development of this research, whose main objective was to
44 determine the most efficient mixing time and its relationship with the properties of fresh and
45 hardened cast-in-place concrete, based on a field study, carried out to determine times and
46 rotation speed of the portable mixers used in the works.

47 2. MATERIALS AND METHODS

48 2.1 Previous field study

51 This stage was aimed to obtain reliable information about mixing times, rotation speeds and
52 the characteristics of the used mixers. Also, direct interviews were applicated to local
53 builders and construction workers for detect those works where cast-in-place concrete was
54 being used, which constituted the size of the population to be observed, using an intentional
55 deterministic sampling. The study was carried out in Chetumal City, located in Mexico's
56 southeastern region, whose population is 151,243 inhabitants [10]. It has sub-humid warm
57 weather most of the year, being the average annual temperature of 26.4° C. The technical
58 data of the portable rotary drum mixer and concrete casting practices were determined by
59 direct observation. Mixing times were measured with a stopwatch from which last material
60 was discharged into the mixer. The technical data were processed in those cases where
61 some external factors modified the continuity of the work, such as workers distractions, lack
62 of material and other delays, in this way the averages of rotation speed and mixing time
63 were obtained for the control specimens. The location of the monitored works in the city
64 territorial extension can be seen in Figure 1.



67
68
69 **Figure 1. Monitored works location**

70 2.2 Materials

71 The used materials were ordinary portland cement, water, and fine and coarse aggregates,
72 both obtained by crushing limestone from a local quarry, whose properties were determined
73 according to ASTM standards [11], summarized in Table 2.
74

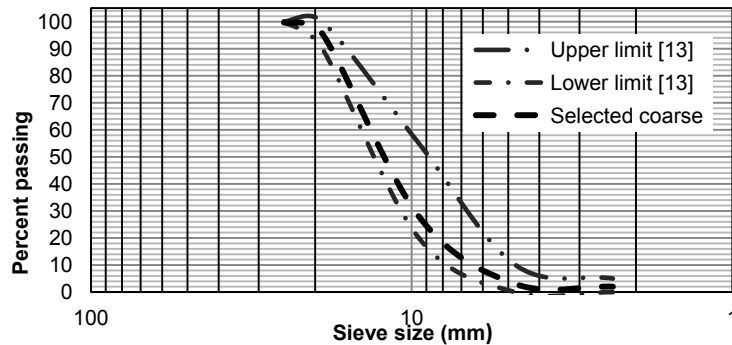
75
76

Table 2. Aggregates properties

Property	Coarse aggregate	Fine aggregate
Loose unit weight (kg/m ³)	1265	1462
Compact unit weight (kg/m ³)	1343	--
Specific gravity	2.5	2.7
Absorption (%)	4.3	1.4
Abrasion (%)	35	--
Maximum size (mm)	19	--
Fineness modulus	--	2.9

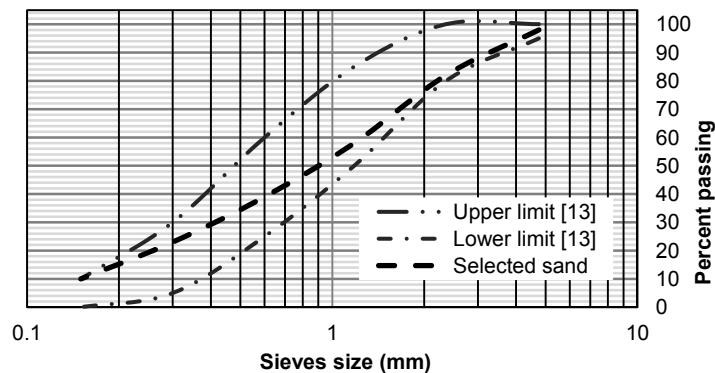
77
78
79
80
81
82
83
84

As expected, the characteristics of the aggregates showed typical unfavorable conditions of the materials of limestone origin [12]. On the other hand, the granulometric study of the coarse aggregate indicated a reduced amount of particles that pass the 9.5 mm sieve (Figure 2). The selected fine aggregate for this investigation had an acceptable granulometry, except for the amount of material that passes the No. 50 sieve equivalent to 50 μm (Figure 3).



85
86
87
88

Figure 2. Granulometry of coarse aggregate



89
90
91
92

Figure 3. Granulometry of fine aggregate

2.3 Experimental Details

93 The selected rotation speeds according the previous field study, were 25, 70, 90, 100, 110,
94 120 and 140 RPM, each with its equivalent mixing time. These values were considered as
95 independent variables; to identify them they were assigned the letter **S** (sample) followed by

96 a consecutive number, where S1 corresponded to the control sample. The dependent
 97 variable was compressive strength (F_c). Mixture design was performed based on ACI
 98 method [14], where the water/cement ratio (w/c) was 0.45 with 75 mm of slump. The relative
 99 amounts of the materials, before daily moisture corrections, are indicated in Table 3. The
 100 fresh concrete tests were slump and trapped air. For F_c tests, cylindrical specimens of 15 x
 101 30 cm were cast, which were subjected previously to a process of moist curing by immersion
 102 for 28 days at 3, 7, 14, 28 and 90 age days.

103
 104 **Table 3. Mixtures design**

Material	Relative amounts (kg/m ³)
Water	205
Cement	456
Coarse aggregate	822
Fine aggregate	862

105

106 **3. RESULTS AND DISCUSSION**

107

108 In the preliminary field study, fourteen works were observed, where the average time for
 109 casting was 0.9 minutes with a rotation speed of 25 RPM in each batch. A rotary drum
 110 portable mixer with 50 kg load capacity and 28 RPM speed was used. This information was
 111 useful to set the concrete mixing time and choose the laboratory equipment. The obtained
 112 results for the fresh concrete, including the environmental temperature during the casting, as
 113 well as the rotation speeds and equivalent mixing times are indicated in Table 4.

114

115

Table 4. Fresh concrete properties

Sample	RPM	Mixing time (min)	Slump (mm)	Trapped air (%)	Environmental Temperature (°C)
S1	25	0.9	50	3.4	27
S2	70	2.5	50	3.1	29
S3	90	3.2	55	3.6	29
S4	100	3.6	40	3.7	27
S5	110	3.9	30	3.2	28
S6	120	4.3	46	3.4	31
S7	140	5.0	40	3.4	31

116

117 As can be seen in Table 4, trapped air varied slightly, with no apparent influence of mixing
 118 time. Regarding the slump, it is observed that all the samples were below the design value,
 119 being more evident in those with longer mixing time. Similar values were found by Gonzalez
 120 et al. [15] when w/c ratios were less than 0.47. The ambient temperature varied in a range of
 121 4 °C without showing any influence on the properties.

122 The F_c results at different ages, revealed a rapid growth tendency, because on the seventh
 123 day, they reached more than 80% of their optimum resistance, which denotes good
 124 efficiency of the mixing process. The sample with the longest mixing time (S7) was the one
 125 that reached the highest F_c at the age of 28 days, 20% more than the control sample (S1),
 126 which can be seen in Figure 4.

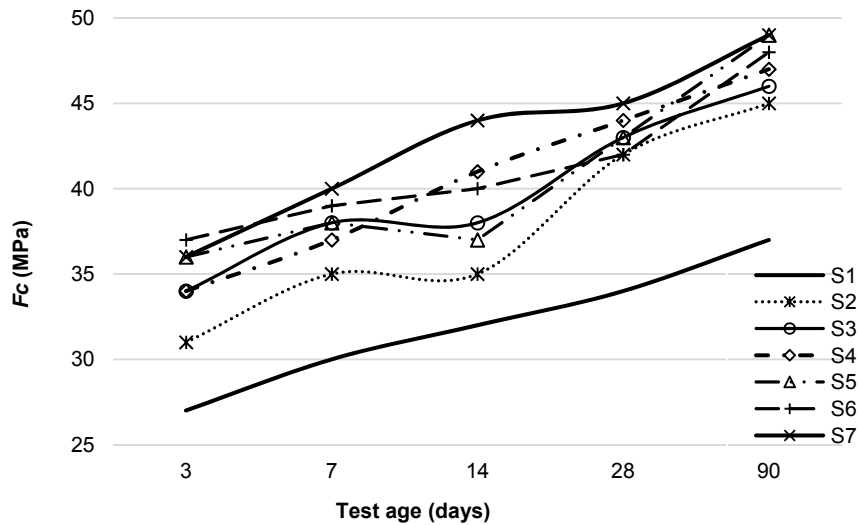


Figure 4. Compressive strength at different ages

These results can be contrasted with the ready-mix concrete data, informed by Kirca et al. [16] and Trejo and Chen [17], who also reported increases in the F_c when the mixing time was increasing. According Equation 1, the real influence of the mixing time on the F_c was determined with an Efficiency Index (EI), which was calculated from the ratio between F_c differentials (ΔF_c) and mixing time differentials (Δt) of each sample under study compared to the control sample.

$$EI = \Delta F_c / \Delta t \quad (1)$$

The complete outcomes at the age of 28 days can be seen in Table 5, where the most recommended mixing time is 2.5 minutes (S_2) according EI .

Table 5. Efficiency index of the samples

Sample	F_c (MPa)	Time (min)	ΔF_c	Δt	EI
S1	34	0.9	--	--	--
S2	42	2.5	8	1.6	5.0
S3	43	3.2	9	2.3	3.9
S4	44	3.6	10	2.7	3.7
S5	43	3.9	9	3.0	3.0
S6	42	4.3	8	3.4	2.4
S7	45	5.0	11	4.1	2.7

Lastly, a statistical analysis for F_c data was carried out. The normality was verified with shape coefficients: -1.85 for asymmetry and -0.18 for kurtosis, which were within the expected range of a normal distribution (± 2). Subsequently, the results for ANOVA showed that $P < .001$. Since the significance was less than .05, indicating the difference between the means of the seven variables or samples under study, a multiple-rank test was performed using the LSD method to identify homogeneous groups among the means [18]. As result, a marked difference was observed between the control samples (S_1) and the rest, a strong

152 similarity between the samples S3, S4, and S5, and some similarity of the samples S6 and
153 S7 with the three previous ones.

154

155 4. CONCLUSIONS

156

157 The present work constitutes one of the first efforts in establishing appropriate mixing times
158 for cast-in place concrete, using high absorption limestone aggregates. According to the
159 results of the research, the following conclusions can be drawn:

160 The mixing time and environmental temperature had no apparent influence on the slump of
161 the mixtures. Trapped air and compressive strength increased slightly with increasing mixing
162 time. In statistical terms, between 3.2 and 3.9 minutes of mixing time, the same quality
163 results are achieved. The most efficient mixing time corresponded to 2.5 minutes with a
164 speed of 28 RPM, which differs from the referenced standards and the common practice
165 established in the previous field study.

166 REFERENCES

167

- 168 1. Mindess S, Young JF, Darwin D. Concrete. 2nd ed. Upper Saddle River (NJ): Prentice
169 Hall. 2003.
- 170 2. NMX C-159-ONNCCE-1999. Industria de la Construcción-Concreto-Elaboración y
171 Curado de Especímenes en el laboratorio. México: Organismo Nacional de
172 Normalización y Certificación de la Construcción y Edificación, S. C. 1999. Spanish.
- 173 3. ASTM C 94-13. Standard Specification for Ready Mixed Concrete. West
174 Conshohocken, (PA): American Society for Testing and Materials. 2013.
- 175 4. ACI 304 R-00. Guide for Measuring, Mixing, Transporting, and Placing Concrete.
176 Farmington Hills (MI): American Concrete Institute. 2000.
- 177 5. NMX C-403-ONNCCE-1999. Industria de la Construcción-Concreto Hidráulico para Uso
178 Estructural. México: Organismo Nacional de Normalización y Certificación de la
179 Construcción y Edificación, S. C. 1999. Spanish.
- 180 6. ACI Committee 318. Building Code Requirements for Structural Concrete and
181 Commentary. Farmington Hills (MI): American Concrete Institute. 2014.
- 182 7. Neville AM, Brooks JJ. Tecnología del concreto. 1st ed. México: Trillas. 2010. Spanish.
- 183 8. Charonnat Y, Beitzel H. Efficiency of concrete mixers towards qualifications of mixers.
184 1997; Mater Struct, RILEM, Supplement March. 32-28.
185 <https://doi.org/10.1007/BF02539273>.
- 186 9. Trejo D, Chen J. Effects of Extended Discharge Time and Revolution Counts for Ready-
187 mixed Concrete. Research Project SPR. Final Report. Oregon State University. 2014.
- 188 10. Instituto Nacional de Estadística y Geografía. Censo de Población y Vivienda 2010.
189 2013. <http://www.inegi.org.mx/est/contenidos/proyectos/ccpv/cpv2010/default.aspx>.
190 Spanish.
- 191 11. ASTM Book of Standards, Construction: Concrete and Aggregates, American Society
192 for Testing and Materials, West Conshohocken, PA, USA, 2010.
- 193 12. Trejo-Arroyo DL, Acosta KE, Cruz JC, Valenzuela-Muñiz AM, Vega-Azamar RE,
194 Jiménez LF. Influence of ZrO₂ Nanoparticles on the Microstructural Development of
195 Cement Mortars with Limestone Aggregates. Appl. Sci. 2019; 598(9): 12.
196 <https://doi.org/10.3390/app9030598>
- 197 13. ASTM C 33-08; Standard Specification for Concrete Aggregates, American Society for
198 Testing and Materials, West Conshohocken, PA, USA, 2008.

- 199 14. ACI 211.1; Standard Practice for Selecting Proportions for Normal, Heavyweight and
200 Mass Concrete, American Concrete Institute, Farmington Hills, MI, USA, 1998.
- 201 15. González-Díaz E, Jaizme-Vega E, Jubera-Pérez J. Assessment of the influence of the
202 effective water-cement ratio on the workability and strength of a commercial concrete
203 used for the construction of concrete caissons. Rev. Constr. 2018; 32(2): 239-231.
204 <https://doi.org/10.7764/RDLC.17.2.231>.
- 205 16. Kirka Ö, Turanlı L, Erdoğan T. Effects of Retempering on Consistency and Compressive
206 Strength of Concrete Subjected to Prolonged Mixing. Cem. Concr. Res. 2002; 32(3):
207 445-441. [https://doi.org/10.1016/S0008-8846\(01\)00699-8](https://doi.org/10.1016/S0008-8846(01)00699-8).
- 208 17. Trejo D, Chen J. Influence of Mixing Time on Fresh and Hardened Concrete
209 Characteristics. ACI Mater. J. 2015; 112 (6): 754-745.
210 <https://doi.org/10.14359/51687396>.
- 211 18. Montgomery DC. Diseño y Análisis de Experimentos, Limusa Wiley: México, 2011.
212 Spanish.
213



© 2019 by the authors. Submitted for possible open access publication under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).

214