

**THE DESIGN AND CONSTRUCTION OF AN INTELLIGENT DEVICE
FOR COATING FLAWS AND CRACK DETECTION IN PIPELINES**

Abstract: *The major pollutant induced by pipeline failure in Oil and Gas industry in Nigeria has been mitigated over the years using non-destructive techniques like liquid penetrant, magnetic particles, radiographic, ultrasound and eddy current testing. The eddy current technique's advantages over the other testing devices remains to best suitable in the design and construction of the devices due to the nature of the pipeline materials. For this present work, a pre-test-post-test experimental design was used to test device on a defect free pipe and a pipe with machined defects of known dimensions and different orientation (longitudinal and axial) after construction. The defect detection was done using electromagnetic technique of eddy current by exciting a coil with power supply and placed close to pipe surface as a micro-controller was used to track irregularities on the material surface by computer systems. The device set up for the test was a coil with a power supply of a DC battery connected with micro-controller of a quantization level of 4.88mV. For visual display, result obtained has showed no variation in the amplitude of the pulse as demonstrated by a pipe with no defect while variations (deeps) occurred in the pipe with defects as the coil was traversed over the defect. The orientation had no significant effects on the sensitivity and effectiveness of the device. Results validation was done using a non-destructive technique by visual inspection. Thus, device has shown its effectiveness in detecting defects irrespective of the orientation. Similarly, the size of the defects is a determinant in the amplitude variation of the pulse displayed which implies at higher sensitivity, a high frequency is required.*

Key-words: Eddy Current; DC Battery; Micro Controller; Crack Detection; Pipeline Failure; Pipeline Testing; Non-Destructive Technique; Quantization Level.

1.0 INTRODUCTION

1.1 Background of the Study

It has been established that pipelines happened to be about the safest and most economical (in terms of energy usage) means for transporting products over any distance [1]. A high range of products from non-hazardous products like water to highly inflammable products like petroleum products are transported with pipelines [2]. The safety and integrity of pipelines are a matter of principal importance due to the highly inflammable nature of some of its transported substances [3]. Should a pipeline fail, the transported content can cause extensive environmental damage and also affect the population living and working by the pipeline. Furthermore, pipeline failure is linked with repair and excavation costs, cleaning costs, and loss of content [4]. **The suspected origin of pipe failure was usually detected using a non-destructive technique, stress corrosion cracking (SCC) were observed on the failed pipe. It cost the accompany a lot of millions of dollars in cleaning up the polluted area [5].** Thus, this project entails the **militation** against such pollution caused by flaws leading to failure of pipelines by adopting a suitable technique like eddy current non-**destruction** testing approach.

42 **1.2 The Eddy Current Testing**

43 Eddy current testing (ECT) technique is a widely applied non-destructive test (NDT) to detect defects and
44 access structural reliability in materials (pipelines) in various in sheet metal industries [6]. Their testing
45 technique has nearly been perfected to detect cracks, sub-surface and coating flaws [7] using the
46 electromagnetic principle. The range of thickness that ECT can handle is usually from the level of
47 micrometres to the level of millimetres. The changes in the properties of the coil in conductivity and
48 permeability condition when in contact with the material are detected by the eddy current testing device
49 [8]. The substitution of the probes with the ring of coils will enable the detection of possible surface
50 defects without pipeline obstructions [9]. The choice of check parameters should be done with a deep
51 understanding of the nature and technique of flaws. The device can handle a wide range of flaws such as
52 coating flaws, cracks and so on. The in-depth understanding of this mentioned flaws gave birth to the
53 non-destructive techniques, which is useful in the detection and identification of defects [10]. Thus, the
54 present work design construct and test intelligent device with options for visual display benchmarking
55 against existing non-destructive techniques for testing flaws, identified and implemented algorithms to
56 detect coating flaws and cracks in pipeline structures in the intelligent device [11].

57 **1.3 Crack Induced due to Stress Corrosion**

58 Early detection of cracks induced by stress corrosion cracking and coating flaws will mitigate against the
59 disastrous and sudden failure of pipelines [12]. Nigeria's oil and gas industry has been plagued in recent
60 years with spillage which has caused grave environmental pollution over the year and its estimated to cost
61 about \$614billion and may span through a period of about 30years to clean up the affected environment
62 [13].

63 This proposed device is unlike the existing intelligent pig which is cumbersome, requires high level of
64 technical know-how and needs to be deployed in the pipe to flow with the fluid content of the pipe hereby
65 obstructing operation of the pipe [14]. This has several advantages ranging from portability, affordability
66 and versatility while it does not require high level of technical know-how to interpret the results. In a
67 country like Nigeria with a pipeline network of length 4226km (approximately) for just crude oil and
68 natural gas alone spanning through most part of the country it is essential to develop a device to help in
69 the regular inspection of this pipeline network [15].

70 **1.4 Non-Destructive Test Techniques for Pipelines**

71 The non-destructive techniques are majorly used for research in mechanics of materials and maintenance
72 check in the industry, this technique doesn't in any way affect the structure of the material [16]. The most
73 widely used non-destructive techniques that would be reviewed in the paper are electromagnetic,
74 ultrasonic and liquid penetrant testing [17]. One of the conventional electromagnetic methods utilized for
75 the inspection of conductive materials like copper, aluminium or steel is eddy current non-destructive
76 testing which as shown in this work to be the most versatile and effective techniques of all the other
77 techniques used for pipeline inspection.

78 When selecting an NDT technique, the first issue to be addressed is the type and size of the defect(s) that
79 must be found as postulated in [18]. This was typically based on experience or, increasingly commonly,
80 on fracture mechanics calculations. Visual inspection by production or maintenance personnel is the most
81 widely applied NDT technique and is often used in conjunction with other methods. It frequently does not
82 involve the purchase of specific NDT equipment. Depicted in Table 1 below are the most commonly used

83 non-destructive techniques and a summary of their capabilities and also their demerits as sourced from
 84 Guriong, et al. [19].

85 **Table 1: Commonly used NDT Techniques**

| Technique | Capabilities | Limitation |
|-------------------------|---|--|
| Visual inspection | Macroscopic surface flaws. | Small flaws are difficult to detect, no subsurface flaws. |
| Radiography | Subsurface flaws | Smallest defect detectable is 2% of the thickness; radiation protection. No subsurface flaws not for porous materials. |
| Dye penetration | Surface flaws | No subsurface flaws not for porous materials |
| Ultrasonic | Subsurface flaws | Material must be good conductor of sound. |
| Magnetic particles | Surface / near surface and layer flaws. | Limited subsurface capability, only for ferromagnetic materials. |
| Eddy current for metals | Surface and near surface flaws | Difficult to interpret in some applications; only for metals. |

86

87 **Table 2: Showing the longitudinal, axial cracks and their dimensions machined on the galvanized pipe.**

| S/N | Longitudinal cracks | | | | Axial cracks | | | | |
|-----|---------------------|-------------|------------|------------|--------------|-------------|------------|------------|----------|
| | Sections | Length (mm) | depth (mm) | Width (mm) | Sections | Length (mm) | depth (mm) | Width (mm) | Sections |
| 1 | 1 | 27 | 0.15 | 2 | 1 | 22 | 0.45 | 1.66 | 1 |
| 2 | | 17 | 0.20 | 1.5 | | 20 | 0.11 | 1.66 | |
| 3 | | 27 | 0.22 | 1.5 | | 22 | 0.32 | 1.86 | |
| 4 | 2 | 27 | 0.16 | 1 | 2 | 24 | 0.70 | 1.86 | 2 |
| 5 | | 28 | 0.25 | 1 | | 22 | 0.21 | 1.66 | |
| 6 | | 26 | 0.45 | 1.8 | | 24 | 0.21 | 1.86 | |
| 7 | | 26 | 0.22 | 1 | | 24 | 0.41 | 1.66 | |
| 8 | | 15 | 0.58 | 2 | | 23 | 0.47 | 1.66 | |

| | | | | | | | | | |
|----|---|----|------|---|---|----|------|------|---|
| 9 | 3 | 15 | 0.16 | 1 | 3 | 23 | 0.35 | 1.68 | 3 |
| 10 | | 18 | 0.25 | 1 | | 23 | 0.34 | 1.66 | |

88 1.5 The Ultrasonic Testing for Pipeline Defects

89 Defects can be detected using the principle of the propagation of sound waves in a material [20]. In the
90 case of ultrasonic testing which is a very competent and reliable non-destructive testing technique, ultra-
91 high-frequency sonic energy above the audible range is used in locating and identifying defects in
92 materials that are at any point in the pipeline materials [21].

93 Research have shown that most ultrasonic testing in pipelines are done within the range of 1 – 5 MHz, but
94 frequency range of 100MHz to 20KHz is used in specialist applications. Both shear and compression
95 waves are mostly used and they detect defects through the change in acoustic impedance produced
96 (product of density and speed of sound) in the path of the ultrasonic beam [17, 22].

97 Ultrasonic testing is commonly used in the industries because of its ease to use, accuracy and its ability
98 not to affect a material in any way for several purposes, one of which is quality control. It is also very
99 useful in testing the integrity of materials used in the formation of pipes [23]. Ultrasonic waves require a
100 medium to transmit its ultrasonic waves because it doesn't transmit well through air, solids or gels. It has
101 been discovered over the years that water or grease would conduct ultrasonic sounds effectively between
102 the transducer and the material to be tested [24]. Devices called pigs have been developed using
103 ultrasonic waves to detect defects in in-service pipelines, this has overcome the problem of getting the
104 transducer into contact with an insulated pipe to be tested because it works from the inside of the pipe
105 were interested in developing a device for assessment of the inner walls of underwater oil pipeline. Lamb
106 waves which is also an option of the waves that could be used for ultrasonic testing is preferred for a very
107 thick material just like the electromagnetic waves within a waveguide [25].

108 1.5.1 Merits and Demerits of Ultrasonic Testing in Pipelines

109 This can be deduced based on comparative or similar studies of ultrasonic testing and its application,
110 likewise that its versatility and flexibility avails it for use on a wide range of materials [21, 23]. It poses
111 no form of environmental hazard with very reliable, accurate and fast subsurface flaws detection when
112 compared to the others [26]. It is important to mention the demerits which could pose certain limitations
113 to the use of this device for defects detection on pipelines. A high level of expertise is required while
114 operating the device and cracks parallel to the direction of the wave travelling through the material would
115 not be detected [27]. It is a very expensive test which also requires couples (water or grease) as a medium
116 for the transducer to transmit and receive waves.

117 1.6 Radiography Testing

118 In Radiography Testing the material to be tested is placed between the radiation source and film or
119 detector [28]. Radiographic image formed is basically a two-dimensional shadow presentation of the
120 concentration of radiation passed through a material [29]. Defects of several forms such as a crack that
121 runs parallel to the beam of radiation reduces the absorption of radiation, this will be seen as a light area
122 in the image produced while an inclusion of higher density than the parent material will appear darker
123 [30]. Radiography tests can be carried out in several different forms and each has its specific applications.
124 Below are different radiography tests. This includes the conventional radiograph which is the most

125 appropriate for when the materials to be tested are not too dense or too thin. These types of radiography
126 are useful in detecting large voids, inclusions, trans-laminar cracks, non-uniform fiber distribution, and
127 fiber mis-orientation such as fiber wrinkles or weld lines [31]. The gamma ray radiography test which is
128 good for dense materials because the gamma rays have shorter wavelengths and the penetrant-enhanced
129 radiography which is employed specifically to detect small matrix cracks and delamination in the material
130 to be tested [32].

131

132 **1.6.1 Varieties of Radiographic Testing Method and Applications**

133 There are varieties of radiographic testing methods for different applications. These methods are film
134 radiography, computed radiography [28], computed tomography [9], and digital radiography [3]. X-ray
135 Computed Tomography (XCT) is a non-destructive technique for visualizing interior features within solid
136 objects, and for obtaining digital information on their 3-D geometries and properties. The great advantage
137 of XCT in comparison with the projection radiology is the 3-D visualized image of the structure while in
138 projection radiology the image is only 2-D. Therefore, the XCT data is readable quickly and simply. XCT
139 will modify the scale of observation from macroscopic to microscopic scale so the results of the XCT
140 method are very reliable [7]. The major disadvantage of radiography is the health hazard posed by
141 radiation [1]. It is expedient to know that radiation imaging method of NDE enjoys an advantage over many
142 other NDE methods in that it is inherently pictorial and interpretation is to some extent intuitive [21].
143 Analyzing and interpreting the images requires skill and experience but the casual user of radiation
144 imaging services can easily recognize the item being imaged and can often recognize discontinuities
145 without expert interpretation. Also, X-ray NDE is not as limited to the type of material it can study, unlike
146 other NDE methods [4]. Radiation methods are suitable for sensing changes in elemental composition. It
147 is especially applicable to finding voids, inclusions and open cracks and is often the method of choice for
148 verification of internal assembly details [20]. Radiation is dangerous and also high voltage is needed to
149 generate most X-rays can be dangerous as well as the difficulty in using heavy shielding materials. Also,
150 radiography is limited in utility for detecting cracks [18]. For a crack to affect the transmission of
151 radiation there must be an opening resulting in a local absence of material. A closed crack is not
152 detectable using radiation. In addition, even when the crack has a finite opening, it will generally only be
153 detectable in a radiograph at certain orientations [3]. Ideally the long dimension of the crack is parallel to
154 the direction of radiation travel, i.e., this maximizes the radiation-crack interaction. Surface defects are
155 often hard to distinguish with 2-D radiography [31]. Finally, they are very expensive and time consuming
156 and require the use of highly trained safety conscious engineers, scientists or technicians.

157 **1.6.2 Other Crack Testing Methods in Pipelines**

158 Several other defect testing methods in pipelines include the use of liquid penetrants for detecting flaws
159 has been validated in several literatures. The penetrant is usually applied by an aerosol and is drawn into
160 small openings by capillary action. Following a dwell time, excess penetrant is removed from the surface
161 and a developer in liquid or powder form is applied in Stander, et. al., [37]. This developer absorbs
162 penetrant drawn from discontinuities. Liquid penetrant inspection is used for testing critical parts and
163 articles in aircraft building, ship building, power and agricultural machine building, in railway transport,
164 and in other branches of industry. The merit and demerits of this method is that Penetrant testing is a
165 simple, inexpensive, and sensitive non-destructive testing method [19]. It allows the inspection of a large
166 variety of materials, component parts, and systems for discontinuities that are open to the surface. Liquid
167 penetrant is portable, it is often used in remote locations. It has been observed that it does not require high

168 level of expertise compared to some other NDT methods, even though careful attention to cleanliness,
169 procedures, and processing time is needed, and also comprehensive knowledge of types of discontinuities
170 that may occur in the parts to be tested.

171 **1.7 The Eddy Current Testing Principle**

172 This testing uses the fact that when an alternating current coil induces an electromagnetic field into a
173 conductive test piece, a small current is created around the magnetic flux field; much like a magnetic field
174 is generated around an electric current. The principle of eddy current is based on electromagnetic
175 induction; this is best captured using the Maxwell equations.

$$176 \qquad \qquad \qquad D = \epsilon E \qquad \qquad \qquad (1)$$

$$177 \qquad \qquad \qquad B = \mu H \qquad \qquad \qquad (2)$$

$$178 \qquad \qquad \qquad J = \sigma E \qquad \qquad \qquad (3)$$

179 The complex parameters in the above equations 1 to 3 are D, B, E, H and J and they represent electric flux
180 density, magnetic flux density, electric field, magnetic field strength and current density respectively with
181 ρ as electric charge density. With additional parameters of ϵ , μ and σ which are electric permittivity,
182 magnetic permeability and electric conductivity. The flow pattern of this secondary current, called an
183 "eddy" current, will be affected when it encounters a discontinuity in the test piece, and the change in the
184 eddy current density can be detected and used to characterize the discontinuity causing that change [36].

185 **2.0 EXPERIMENTAL PROCEDURE**

186 **2.1 Materials and Methods**

187 The extensive steps used in the design and the several tests used for calibration of an intelligent device
188 examined on a carbon steel pipe would be discussed in this chapter. As stated earlier, the primary goal of
189 this present work is to detect coating flaws and surface cracks on pipelines. The system model Figure 3
190 presents a diagram of the basic probe-flaw interaction. There are some parameters, including the magnetic
191 field range, the operating frequency band and sensor dimensions that permit the selection of the most
192 suitable sensor type for eddy current testing. After the broad discussion of the five most commonly used
193 non-destructive techniques, Eddy current proved to be the most appropriate considering the property of
194 the availed test material and the nature of the test to be conducted on it. For effective research and
195 analysis, the system is divided into three modules, namely power source, microcontroller and data
196 acquisition. In addition, the application of the eddy current technique in the device design, the
197 experimental design for the test of the intelligent device and its procedures is well highlighted. The
198 concluding part of this **chapter** will focus on the signal processing of the output data for a good result.

199 **2.2 Coil and Power Source**

200 The power of this system was sourced from a direct current 12V battery which controls supply channel
201 for the individual components. The advantages of using coils as sensors for the eddy currents are the
202 simplicity of their construction, the huge dynamic range and the possibility of focusing the sensor which
203 is confirmed by De Haan, et al., [11]. The coils used as the probe sensor is made of copper wires and
204 circular in design. Special profile encircling probes are designed for researchers and manufacturers to
205 control surface and sub-surface defects in products with special profiles and shapes. The four coils in total
206 are homogenous in dimensions and properties, these coils are connected in series to form a chain round

207 the pipe for easy and complete testing of the pipe. The inner and external diameters of the coils stand at
208 5mm and 15mm respectively. The length of each of the coils are 110mm with resistance of 40Ω and
209 excitation current of 50mA. All this was done to achieve the required sensitivity of the probe which is
210 vital in flaw detection. Tian, et al. [38] took the relationship between coil size and sensitivity into account
211 and proposed a method for reconstructing the flaw in order to determine the crack's depth. The coil had
212 600 number of turns and are connected to the microprocessor where the change in impedance experienced
213 in the coil is filtered to leave only useful signal for processing as shown in Fig. 2 below.
214 The calibration of the device was done to ensure that the coils were sensitive enough to detect defects and
215 to ascertain if the micro controller was able to take the change of the impedance on the coil from analogue
216 to digital for visual display which eases interpretation of the result.

217 2.3.1 The Micro-Controller

218 The micro controller chip was used to receive the analogue signals from the coil and remove noisy signals
219 (through the use of common mode rejection ratio), process and concurrently send signals to the computer
220 system for visual display. Its major constituency is the analogue to digital converter. The two important
221 steps taken by this chip to perform its function includes:

- 222 • **Signal quantization:** This step took the output voltage signal from the coil and the discretized it
223 into resolution signals of 4.88mV. Thus, this can be mathematically shown below

$$224 \text{Quantization level} = \frac{V_{\max} - V_{\min}}{2^L} \quad (4)$$

225 Where L (Number of analogues to digital converter bits) = 10

226 Maximum voltage (V_{\max}) = 5V

227 Minimum voltage (V_{\min}) = 0V

- 228 • **Encoding:** This involves the conversion of resolution signals of 4.88mV into digital resolution.
229 This was done with the use of the Arduino Nano device connected via a USB port to aid the
230 transfer of the digital representation of the signal to the computer system for further review and
231 analysis.

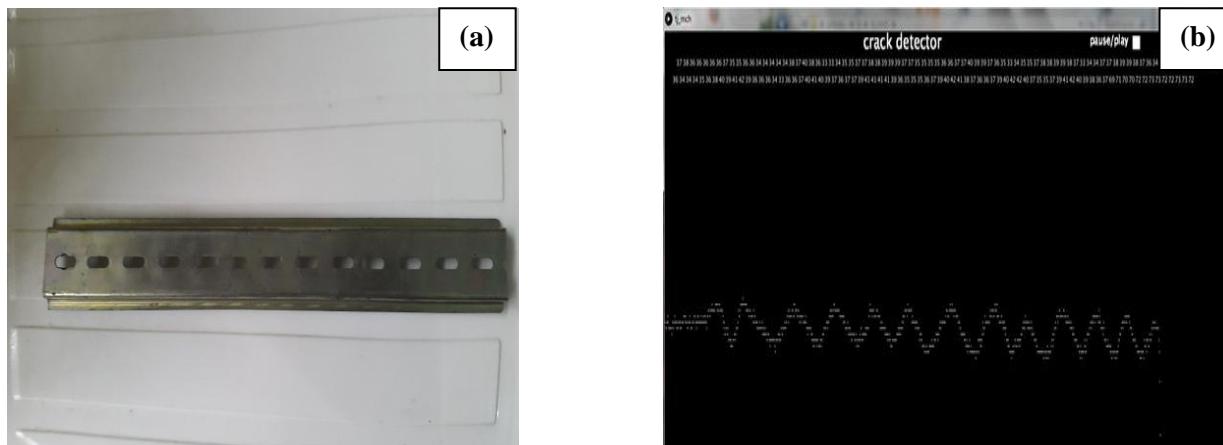
234 2.3.2 Visual Display

235 Several eddy current instruments are available with computer connections that vastly increase their
236 capabilities to search, visualize and analyze eddy current inspection data [34, 35]. Computers systems can
237 receive data from multiple channels and also with real-time processes of the inputs it gets. Some authors,
238 such as Rao et al., [24], Fahmy et al., [31], and Stander et al., [32], have published papers relating to
239 computer-controlled eddy current systems. Interpretation of the test was done with the use of an eddy
240 current device, made simple through an explicit graphical display aided by the Processing 3 software,
241 flexible software in a visual context. This displayed a pulse signal which has a baseline of the value of
242 4.88mV but could change in amplitude for every increase or decrease in the value of the of the baseline
243 signal.

244 2.3.3 Experimental Design for Test

245 The device was initially calibrated with a steel plate 260mm by 35mm with 12 holes machined on it. The
246 holes have dimensions of 12mm by 4mm and are evenly spaced along the surface of the plate with
247 equidistance of 8mm. The display on the screen showed clearly the effect of the holes on the coil that is

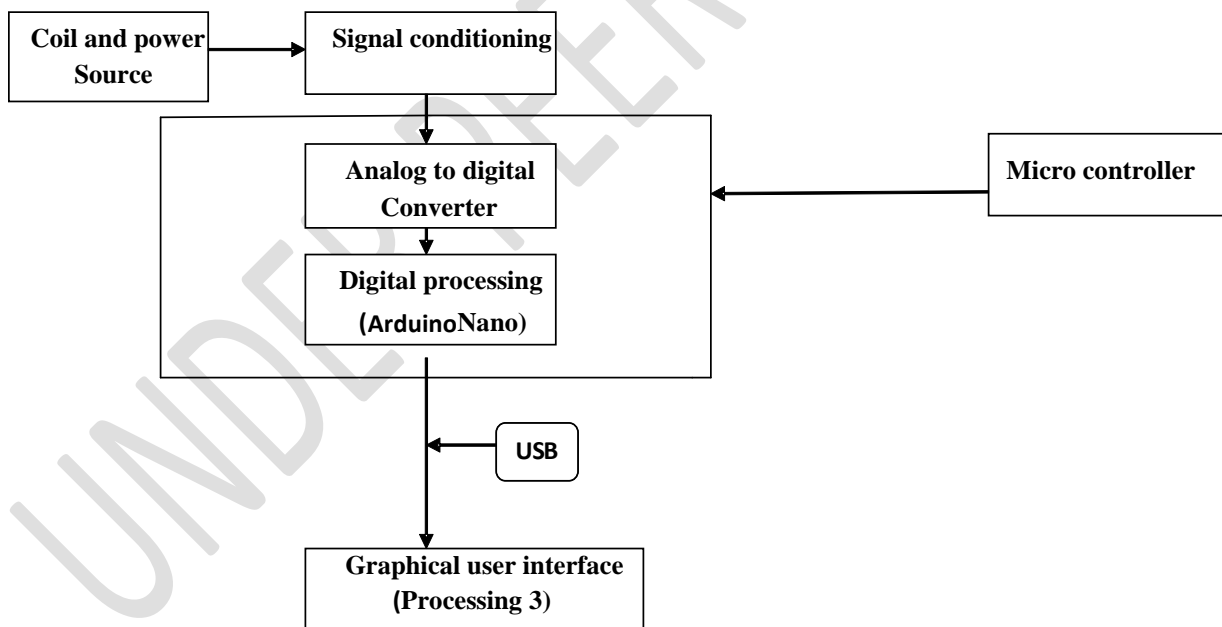
248 been moved along the surface of the plate. The metal plate and also result from the calibration of the
249 device using the steel plate are depicted in Fig. 1 below.



250
251 **Figure 1(a):** The metal plate used to calibrate the device **(b)** Result showing the twelve holes on the tested device

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255 2.4 Designs for Eddy Current Testing Device



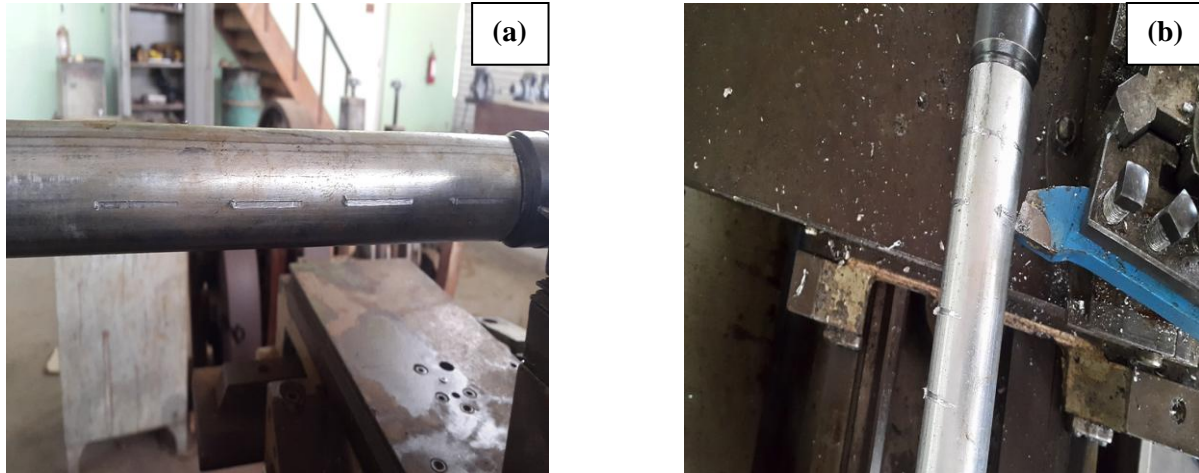
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267 **Fig. 2:** Flow diagram denotes principal for Eddy Current Testing Device

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269 The result from the calibration was validated by doing a visual inspection of the metal plate, this was followed by
270 testing the device on a pipe. Two Galvanized test pipes were purchased and cut into smaller lengths of 300mm with

271 internal diameter of 30mm and external diameter of 31.72mm. These measurements were done with a ruler and
272 digital Vernier caliper respectively while the abrasions machined using the lathe machine. This is done to imitate a
273 pipeline with cracks on it for the device to detect. The galvanized steel pipes were chosen because of its close
274 similarity to the pipeline in terms of the material which is steel with resistivity of $1.43 \times 10^{-7} \rho$ ($\Omega \cdot m$) and
275 conductivity of $6.99 \times 10^6 \sigma$ (s/m). Below are the two orientations of cracks (longitudinal and axial cracks) with their
276 dimensions and also the machining processing that was done on each of the pipes as shown in Fig. 3 below.



277
278 **Figure 3:** Different side view of the tested cracked device (a) Longitudinal (b) Axial

279 3.0 RESULTS AND DISCUSSION

280 This present work was done using an indigenous design for a compact and effective eddy current device
281 and connecting coils in series for outer surface of pipe inspection using eddy current testing device.
282 The non-destructive technique of eddy current testing was the basic principle on which this intelligent
283 testing device was designed and constructed [36, 37]. The device was able to induce eddy current on the
284 pipe (test material) through a coil and also give a visual display of the result from the change in
285 impedance on the coil on computer system software (Processing 3) through a micro controller connected
286 to it. The set up for the device constructed is shown below. This device does not only detect defects but
287 will also help in monitoring and evaluating defects on pipes.

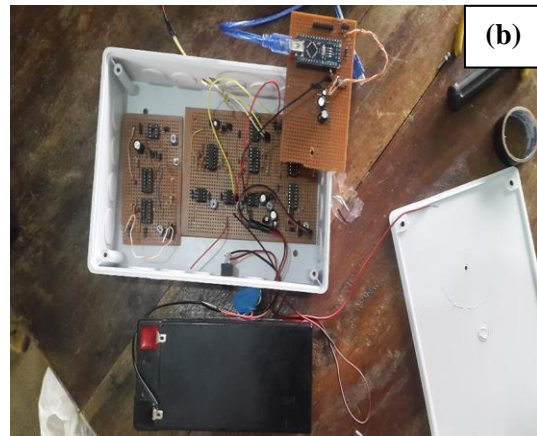
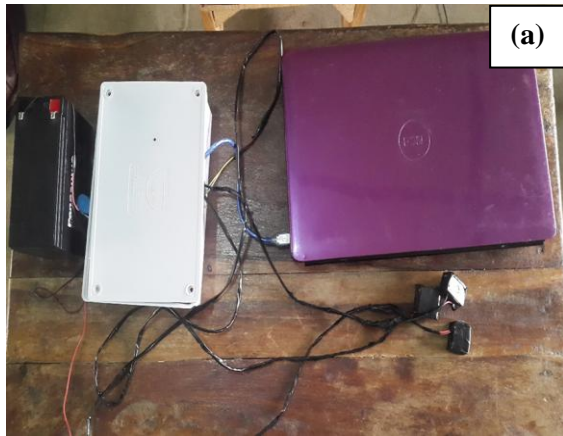
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289 3.1 Defects in Conductive Materials

290 The presence of a defect in a conductive material implies a region where electrical conductivity is null. If
291 electrical currents are generated in the conductive material, in these regions they do not exist and paths
292 are disturbed. In an open surface defect eddy currents can go around it, moving at the same horizontal
293 plane, or can even immerse, passing underneath the crack [38]. Each of these behavioural occurrences
294 depends on the crack length, on the crack depth and on the standard depth of penetration determined by
295 the operating frequency and the electrical conductivity [39]. In this present work, experimental tests were
296 performed on the test pipes containing machined axial and longitudinal defects with the setup in scanning
297 an area over the crack. An operating frequency of 100 Hz was imposed to the excitation coil.

298 3.2 Eddy Current Testing Device

299 The device is basically made up of a circular coil with parameters as earlier stated in the methodology
300 which is powered by a direct current battery and also a micro controller that converts the analogue signals
301 to digital and filters noisy signals [40]. This is connected to a computer system software (Processing 3)
302 which displays the effect of the surface of the pipe on the coils. The complete set up of the eddy current
303 device as shown in Fig. 4 below.



304
305 **Figure 4:** (a) Complete set-up of an eddy current test device (b) The Micro-controller

306 **3.3 Experimental Test Design**

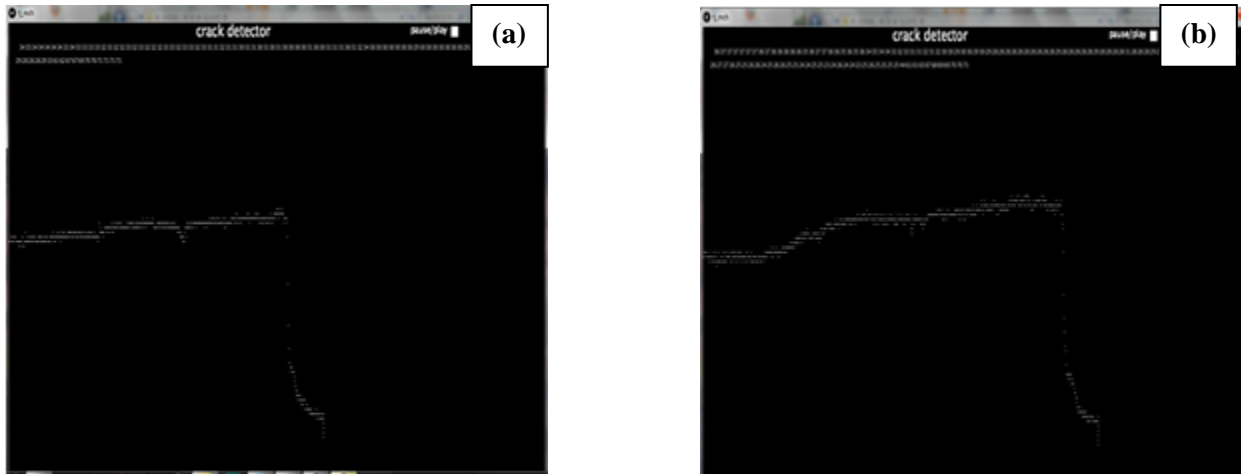
307 A pre-test and post-test experimental design was employed in the testing of galvanized steel pipes. The
 308 pre-test was done on the galvanized pipe after which the post-test was done on a galvanized pipe with
 309 machined defects of both axial and longitudinal orientations as developed in the models in [Chapter 3](#).
 310 First, the result of the pre-test on a defect free pipe is presented showing the response of the coil to the
 311 impedance encountered on the pipe. Second, the result of the post-test on the pipe with both the
 312 longitudinally and axially machined defects showing the response of the coil to the impedance caused by
 313 the defects. Then lastly the test result from a half-coated pipe is also presented. All the cases mentioned
 314 involves scanning the surface of the pipe with the coils. A very strong algorithm was also developed to
 315 filter, magnify output response and also visually display an easy to interpret result. Validation was carried
 316 out using a Non-destructive technique.

317 **3.3.1 Test on Defect Free Galvanized Steel Pipe**

318 This test shows the response of the coil on a defect free pipe. At the start of the test lift off caused a little
 319 change in the pulse signal but as the test progressed it was eliminated by maintaining a constant distance
 320 between the coil and the pipe. The relatively straight pulse signal shown on the screen of the computer
 321 system was expected as the impedance on the coil was relatively constant and was not and altered in
 322 anyway due to absence of any form of defect on the test pipe. Shown below in Fig. 5 and Fig. 6 are the
 323 visual display of the test conducted using the Processing 3 software on a computer system. The numbers
 324 at the top of the screen is just to show the numerical values of the nverse of the change in impedance on
 325 the coil which is in line with the pulse signal displayed.



326
327 **Figure 5:** Result from the tested done galvanized pipe (a) without defects (b) with longitudinal defects in section 1



328
329 **Figure 6:** Result from the tested done galvanized pipe with longitudinal defects in (a) section 2 (b) section 3

330 3.3.2 Test on axial Cracks on a Galvanized steel pipe

331 During the post-test carried out on the galvanized steel pipe at the first section lift off was completely
 332 eliminated which gave a more regular pulse signal compared to the longitudinal defects test. Pulse signal
 333 showed significant low amplitude at the points where the coil encountered defects which was a strong
 334 indication. The test on the second section showed also complete elimination of lift off with the pulse
 335 signal regular till defects were encountered by the coil. This was indicated distinctively by the low
 336 amplitude that was seen on the display. The third test carried out in the third section of the pipe also
 337 showed no visible lift off on the display. The pulse signal showed the expected low amplitude at the
 338 points of defects. The visual display of the results can be seen from Fig. 7 below, also showing the
 339 numerical values at the top of each of the display which is the inverse of the impedance on the coil as the
 340 test was been carried on and it is in line with the pulse signal displayed.



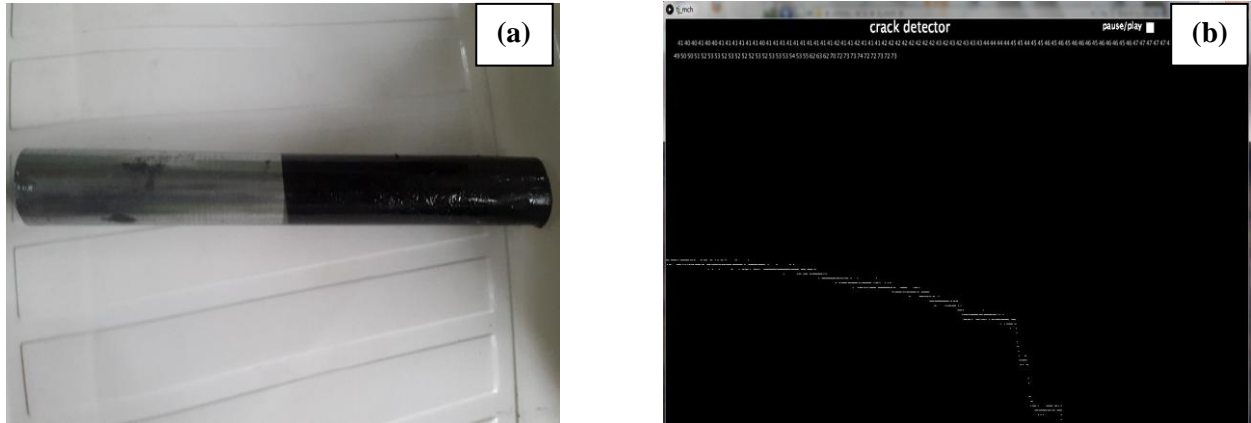
341
342 **Figure 7:** Result from the tested done galvanized pipe with axial defects in (a) section 1 (b) section 2 (c) section 3

343 3.3.3 Test on Coating Flaws on a Galvanized Steel Pipe

344 Coating flaws which is function of the variation in the thickness of coats on a pipe to keep it from rusting
 345 was also detected by testing the device on a pipe that was half coated with gloss paint as shown in Fig.
 346 8(a) and the result from this test can be seen in the displayed in Fig. 8(b) below. There was no lift off
 347 experienced during the test and the test was done from the part not coated to the part coated. The gradual
 348 low amplitude on the pulse signal was an indication of gradual increase in the impedance which is as a
 349 result of the increase in thickness of the area covered by the coil as it moves on the surface of the pipe.

350 **3.4 Validate of Test Device**

351 All the result of the defects tested for on the galvanized pipe as depicted in was validated by using a non-
352 destructive test of visual inspection and it was validated that though the change in pulse signal was not
353 relative to the size of the defects being detected due to low sensitivity of the coil but it was effective in
354 detection.



355
356 **Figure 8(a):** Showing a half-coated pipe tested for coating flaws **(b)** result of test galvanized pipe with coating flaws

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UNDER PEER REVIEW

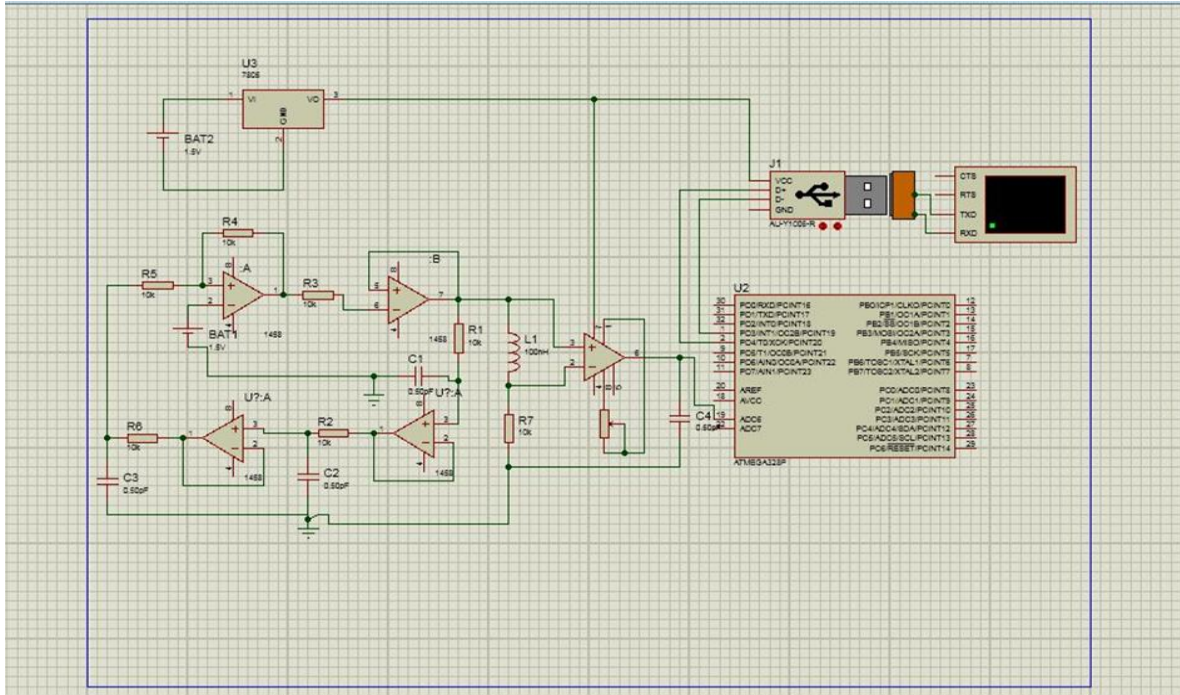


Figure 9: Showing the circuit diagram for the micro controller

4.0 CONCLUSION

This present study gives a solution from the experimental test result that was done on pipelines with longitudinal defects, axial defects and coating flaws. The results confirmed that the designed and constructed intelligent device is able to detect these types of defect or flaws.

From the present experimental investigation, the following conclusions can be made:

- The detection rate for this device on these types of defect is relatively high and reliable. This indicates the proposed intelligent device is sensitive for different defect orientations and nature.
- Detailed analysis on the signals for coating flaws, axial and longitudinal defects shows that the indicating change in amplitude of the pulse signal is not affected by the orientation or nature of the defect.
- Comparing the result from the calibration to that of the test it can be deduced that different sizes of defect generate different pulse signal response, which is useful for defect classification.
- The experimental design validated by the visual inspection method of non-destructive techniques shows the effectiveness of the device.

5.0 REFERENCES

- [1] Carvalho, A. A., Robello, J., Souza, M., Segrilo, L. and Soares, S. (2008). Reliability of Non-destructive Test Techniques in the Inspection of Pipelines used in the Oil Industry, International Journal of Pressure Vessels and Piping. Elsevier Limited, Vol. 85, No. 11, pp. 745–751. doi: 10.1016/j.ijpvp.2008.05.001.
- [2] Chesnokova, A. A., Kalayeva, S. Z. and Ivanova, V. A. (2017). Development of a Flaw Detection Material for the Magnetic Particle Method, Journal of Physics: Conference Series, Vol. 881, No. 1, pp. 120-122.

- 388 Available at: <http://stacks.iop.org/1742-6596/881/i=1/a=012022>.
- 389 [3] Bernieri, A., Betta, G. and Ieee, M. (2000). Metrological Characterization of an Eddy-Current-Based System,
390 pp. 1608–1611.
- 391 [4] Chevil, K. (2015). Investigation of Corrosion and Crack Morphology Behavior under Disbonded Coatings on
392 Pipelines. Doi: 10.1017/CBO9781107415324.004.
- 393 [5] Filipe, R. C. M. (2015). Eddy Current Method for the Assessment of Crack Depths in Metallic
394 Non-Ferromagnetic Plates, Publishes Thesis for Master Degree in Aerospace Engineering, Portuguese Science
395 and Technology University (FCT), Portugal.
- 396 [6] Darvell, B. W. (2018). Radiography, Materials Science for Dentistry, Woodhead Publishing Series in
397 Biomaterials, Tenth Edition, pp. 665–698. Doi: <https://doi.org/10.1016/B978-0-08-101035-8.50026-2>
- 398 [7] Rifai, D., Abdalla, A. N., Khamsah, N., Aizat, M. and Fadzli, M. (2016). Subsurface Defects Evaluation using
399 Eddy Current Testing, Indian Journal of Science and Technology, Vol. 9, No. 9., pp. 1-10.
400 Doi: 10.17485/ijst/2016/v9i9/88724.
- 401 [8] García-Martín, J., Gómez-Gil, J. and Vázquez-Sánchez, E. (2011). Non-Destructive Techniques Based on Eddy
402 Current Testing, Sensors, Vol. 11, No. 3, pp. 2525–2565. Doi: 10.3390/s110302525.
- 403 [9] Michaels, J. E. (2008). Detection, Localization and Characterization of Damage in Plates with an In-situ Array
404 of Spatially Distributed Ultrasonic Sensors, Vol. 1, No. 17. Doi: 10.1088/0964-1726/17/3/035035..
- 405 [10] Glazkov, Y. A. (2012). Evaluation of Material Quality for Liquid-Penetrant Inspection Based on the Visibility
406 of the Indicator Patterns of Flaws, Russian Journal of Non-destructive Testing, Vol. 48 No. 4, pp. 208–217.
407 Doi: 10.1134/S1061830912040067. .
- 408 [11] De Haan, V. O. and De Jonga., P. (2006). Towards Material Characterization and Thickness Measurements
409 using Pulsed Eddy Currents implemented with an Improved Giant Magneto Resistance Magnetometer, Econdt,
410 pp. 1–8. Available at: <http://citeseerx.ist.psu.edu/viewdoc/summary?doi=10.1.1.159.3424>.
- 411 [12] Jin-Su B. and Sang-Young K. (2001). Hot Wire Inspection using Eddy Current, Proceedings of the 18th IEEE
412 Instrumentation and Measurement Technology Conference. Rediscovering Measurement in the Age of
413 Informatics (Cat. No.01CH 37188). IEEE, pp. 962–965. doi: 10.1109/IMTC.2001.928222.
- 414 [13] Yokohama, K., Onda, T. and Nagasaka, T. (2006). Environmental Assessment of Land-fill Mining by using
415 Dynamic Extension of Waste Input-Output Analysis, Journal of Life Cycle Assessment, Japan, Vol. 2, No. 1,
416 pp. 73–79. Doi: 10.3370/lca.2.73.
- 417 [14] Yamada, S., Chomsuwan, K. and Iwahara, M. (2006). Application of Giant Magnetoresistive Sensor for Non-
418 destructive Evaluation, 5th IEEE Conference on Sensors. IEEE, pp. 927–930.
419 Doi: 10.1109/ICSENS.2007.355618.
- 420 [15] Achebe, C. H., Nneke, U. C. and Anisiji, O. E. (2017) ‘Analysis of Oil Pipeline Failures in the Oil and Gas
421 Industries in the Niger Delta Area of Nigeria’, (July 2012).
- 422 [16] Verma, S. K., Bhadauria, S. S. and Akhtar, S. (2013). Review of Nondestructive Testing Methods for
423 Condition Monitoring of Concrete Structures.
- 424 [17] Glazkov, Y. A. (2012). Evaluation of Material Quality for Liquid-Penetrant Inspection Based on the Visibility
425 of the Indicator Patterns of Flaws, Russian Journal of Non-destructive Testing, Vol. 48 No. 4, pp. 208–217.
426 Doi: 10.1134/S1061830912040067.
- 427 [18] Mgonja, C. T. (2017). Evaluation on Use of Industrial Radiography for Weld Joints Inspection in Tanzania,
428 Vol. 8, No. 5, pp. 65–74.
- 429 [19] Guirong, X., Xuesong, G., Yuliang, Q. and Yan, G. (2015). Analysis and Innovation for Penetrant Testing for
430 Airplane Parts, Procedia Engineering, Elsevier, Vol. 99, No. 1 pp. 1438-1442.
431 Doi: 10.1016/j.proeng.2014.12.681
- 432 [20] Wilkinson, S. and Duke, S. M. (2014). Comparative Testing of Radiographic Testing, Ultrasonic Testing and
433 Phased Array Advanced Ultrasonic Testing Non Destructive Testing Techniques in Accordance with the AWS
434 D1.5 Bridge Welding Code BDK84-977-26, pp. 38.
- 435 [21] Shull, P. J. (2002). Non-destructive Evaluation: Theory, Techniques, and Applications. Available at:
436 [http://allaboutmetallurgy.com/wp/wp-content/uploads/2016/11/Nondestructive-Evaluation-Theory-Techniques-](http://allaboutmetallurgy.com/wp/wp-content/uploads/2016/11/Nondestructive-Evaluation-Theory-Techniques-And-Applications_By_Peter_J_Shull.pdf)
437 [And-Applications_By_Peter_J_Shull.pdf](http://allaboutmetallurgy.com/wp/wp-content/uploads/2016/11/Nondestructive-Evaluation-Theory-Techniques-And-Applications_By_Peter_J_Shull.pdf).
- 438 [22] Xu, B. and Hong, H. (2014). Intelligent Eddy Current Crack Detection System Design Based On Neuro-
439 Fuzzy Logic Concordia University Examiner.
- 440 [23] Alobaidi, W. M., Alkuam, E. A., Al-Rizzo, H. M. and Sandgren, E. (2015). Applications of Ultrasonic
441 Techniques in Oil and Gas Pipeline Industries: A Review, American Journal of Operations Research, Vol. 5,
442 No. 4, pp. 274–287. Doi: 10.4236/ajor.2015.54021
- 443 [24] Rao, B. P. C., Raj, B., Jayakumar, T., Kalyanasundaram, P. and Arnold. W. (2001). A New Approach for

- 444 Restoration of Eddy Current Images, *Journal of Nondestructive Evaluation*, Springer Link, Vol. 20,
445 No. 2, pp. 61–62. Doi: 10.1023/A:1012292124404
- 446 [25] Zhou, H. T., Hou, K., Pan, H. L., Chen J. J. and Wang, Q. M. (2015). Study on the Optimization of Eddy
447 Current Testing Coil and the Defect Detection Sensitivity, *Procedia Engineering*, Vol. 130, pp. 1649–1657.
448 Doi: 10.1016/j.proeng.2015.12.331.
- 449 [26] Yi n, W., Binns, R., Dickinson, S. J. and Davis, Claire. (2008). Analysis of the Liftoff for Effect of Phase
450 Spectra for Eddy Current Sensors, *Instrumentation and Measurement*, IEEE Transactions, Vol. 1, No. 56,
451 pp. 2775–2781. Doi: 10.1109/TIM.2007.908273
- 452 [27] Rifai, D., Abdalla, A. N., Khamsah, N., Aizat, M. and Fadzli, M. (2016). Subsurface Defects Evaluation using
453 Eddy Current Testing, *Indian Journal of Science and Technology*, Vol. 9, No. 9., pp. 1-10.
454 Doi: 10.17485/ijst/2016/v9i9/88724.
- 455 [28] Yahaghi, E., Movafeghi, A. and Mohmmadzadeh, N. (2015). Enhanced Radiographic Imaging of Defects in
456 Aircraft Structure Materials with the Dehazing Method, *Non-destructive Testing and Evaluation*. Taylor and
457 Francis, Vol. 30, No. 2, pp. 138–146. Doi: 10.1080/10589759.2015.1018254.
- 458 [29] Sigma Industrial Service. (2018). Liquid Penetrant. Available at: [http://sigmaindustrial.co.za/liquid-penetrant-](http://sigmaindustrial.co.za/liquid-penetrant-inspection)
459 inspection (Accessed: 14 August 2018).
- 460 [30] ASNT (2017) No Title, Introduction to NDT. Available at:
461 <https://www.asnt.org/MinorSiteSections/AboutASNT/Intro-to-NDT>
- 462 [31] De Beer, F. C. (2015). Neutron- and X-ray Radiography or Tomography: Non-destructive Analytical Tools for
463 the Characterization of Nuclear Materials, *Journal of the Southern African Institute of Mining and Metallurgy*.
464 The Southern African Institute of Mining and Metallurgy, Vol 115, No. 10, pp. 913–924.
465 Doi: 10.17159/2411-9717/2015/v115n10a3.
- 466 [32] Fahmy, M. N. I., Hashish , E. A., Elshafiey. I. and Jannound, I. (2000). Advanced System for Automating
467 Eddy-Current Non-destructive Evaluation, *Proceedings of the Seventeenth National Radio Science*
468 *Conference*. 17th NRSC'2000 (IEEE Cat. No.00EX396), Minufiya, Egypt, 2000, pp. H5/1-H5/8.
469 Doi: 10.1109/NRSC.2000.838977.
- 470 [33] Abushanab, W. (2013). Oil Transmission Pipelines Condition Monitoring Using Wavelet Analysis and
471 Ultrasonic Techniques, *Engineering*, Vol. 5 No. 6, 2013, pp. 551-555. Doi: 10.4236/eng.2013.56066.
- 472 [34] Kasai, N., Takada, A., Fukuoka, K. and Aiyamam H. (2011). Quantitative Investigation of a Standard Test
473 Shim for Magnetic Particle Testing, *NDT and Elsevier International*, Vol. 44, No. 5, pp. 421–426.
474 Doi: 10.1016/j.ndteint.2011.03.004.
- 475 [35] Yang, R., Yunze, H. and Zhang, H. (2016). Progress and Trends in Nondestructive Testing and Evaluation for
476 Wind Turbine Composite Blade, *Journal of Renewable and Sustainable Energy Review*, Elsevier Publication,
477 Vol. 60, No. 1, pp. 1225-1250, DOI: 10.1016/j.rser.2016.02.026
- 478 [36] Yu, Y. T., Zou, Y., Al-Hosani, M. and Tian G. Y. (2017). Conductivity Invariance Phenomenon of Eddy Current
479 NDT: Investigation, Verification, and Application, *IEEE Transactions on Magnetics*, Vol. 53, No. 1, pp. 1–7.
480 Doi: 10.1109/TMAG.2016.2616328.
- 481 [37] Stander, J. (1997). A Novel Multi-Probe Resistivity Approach to Inspect Green- State Metal Powder
482 Compacts, Vol. 16, No. 4, pp. 205–206.
- 483 [38] Tian, G., Li, Y. and Mandache, C. (2009). Study of Lift-Off Invariance for Pulsed Eddy-Current Signals,
484 *Magnetics*, IEEE Transactions, Vol. 1, No. 45, pp. 184–191.
- 485 [39] Yokohama, K., Onda, T. and Nagasaka, T. (2006). Environmental Assessment of Land-fill Mining by using
486 Dynamic Extension of Waste Input-Output Analysis, *Journal of Life Cycle Assessment*, Japan, Vol. 2, No. 1,
487 pp. 73–79. Doi: 10.3370/lca.2.73.
- 488 [40] Rocha, T., Pasadas, D., Ribeiro, A. L. and Ramos, H. M. (2012). Characterization of Defects on Rivets using a
489 Eddy Current Technique with GMRs, *IEEE International Instrumentation and Measurement Technology*
490 *Conference Proceedings*, Graz, pp. 1640-1644. Doi: 10.1109/I2MTC.2012.6229389

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